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Simulation of Fiber Fuse Phenomenon in Single-Mode Optical Fibers

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Additional information is available at the end of the chapter

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1. Introduction

By utilizing dense wavelength-division-multiplexed (DWDM) transmission systems using an optical-fiber amplifier, large amount of data can be exchanged at a rate of over 60 Tbit/s [1]. In connection with this achievement, the danger of the “fiber fuse phenomenon” occurring has been pointed out. This occurs when high-power (W order) optical signals are transmitted in an optical-fiber cable [2].

The fiber fuse phenomenon was first observed in 1987 by British investigators [3]–[6]. A fiber fuse can be generated by bringing the end of a fiber into contact with an absorbing material, or melting a small region of a fiber by using an arc discharge of a fusion splice machine [3]. If a fiber fuse is generated, an intense blue-white flash occurs in the fiber core, and this flash propagates along the core in the direction of the optical power source at a velocity on the order of 1 m/s (see Figure 1). Fuses are terminated by gradually reducing the laser power to provide a termination threshold at which the energy balance at a fuse is broken.

When a fiber fuse is generated, the core layer in which the fuse propagates is seriously damaged, and the damaged fiber cannot be used in an optical communication system. The damage is made manifest by periodic or nonperiodic bullet-shaped cavities left in the core [7]–[13]. It was found that molecular oxygen was released and remained in the cavities while maintaining high pressure (about 4 atmospheres) at room temperature [4].

Several review articles [14], [15], [16] and a book [17] have been recently published, which cover many aspects of the current understanding of the fiber fuse.

Most experimental results of fiber fuse generation have focused on an intensity of 0.35–25 MW/cm² [3]–[13], [18]–[39]. This is many orders of magnitude below the intrinsic damage limit for silica, which exceeds 10 GW/cm² [3]. The threshold power for an SMF required to generate and/or terminate a fiber fuse was estimated at about 1.0 [7], 1.19 [37], 1.33 [37], and 1.4 W [30] at $\lambda_0 = 1.064, 1.31, 1.48, \text{ and } 1.56 \mu\text{m}$, respectively.

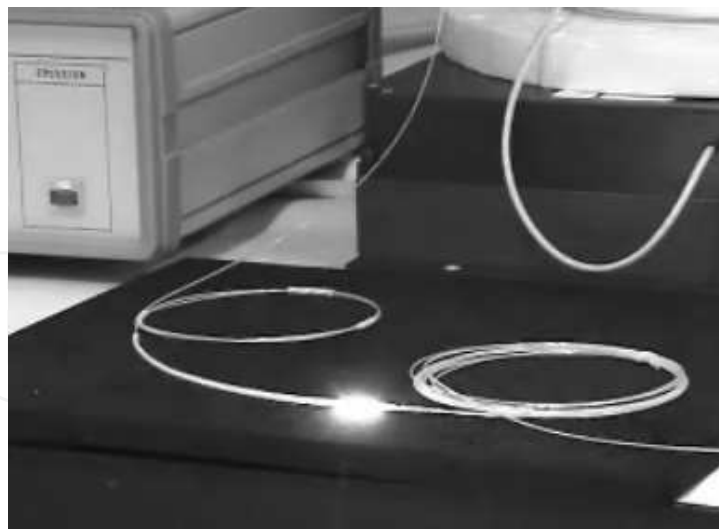


Figure 1. Fiber fuse phenomenon.

On the other hand, the fiber fuse effect in a microstructured optical fiber, in which thirty air holes are arranged around the fiber center, was reported by Dianov *et al.* [40]. No propagation of the fiber fuse was observed at the power of ≤ 3 W and $\lambda_0 = 0.5 \mu\text{m}$. This threshold power (3 W) was an order of magnitude higher than that of a conventional fiber. They also reported that the propagation of the fiber fuse was not observed when the laser light of up to 9 W and $\lambda_0 = 1.064 \mu\text{m}$ entered in the microstructured optical fiber.

It has recently been reported that a hole-assisted fiber (HAF) [41], in which several air holes are arranged near the core of the optical fiber, exhibits high tolerance to fiber fuses [42]–[51]. The fiber fuse propagation in a HAF is affected by both the diameter of an inscribed circle linking the air holes (D_{hole}) and the diameter of the air hole (d_h) (see Figure 2).

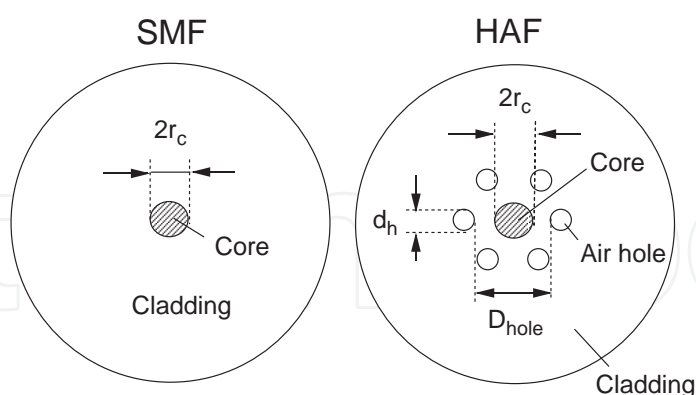


Figure 2. Schematic view of SMF and HAF.

No propagation of fiber fuse was observed in HAFs with $d_h = r_c = 4.5 \mu\text{m}$ and a ratio R_h of the D_{hole} to the core diameter ($2 r_c$) of 2 or less when the laser power P_0 of 13.5 and/or 15.6 W at $\lambda_0 = 1.48 + 1.55 \mu\text{m}$ was incident to HAFs [43], [45], [46].

Takenaga *et al.* investigated the power dependence of penetration length at a splice point of SMF and the HAF with d_h of about 16.3 – $16.9 \mu\text{m}$ and R_h of about 2.3, called “HAF2₊” [42],

[47]. The fiber fuse propagation immediately stopped in HAF2₊ for P_0 of 2.0–8.1 W at $\lambda_0 = 1.55 \mu\text{m}$, where the penetration length was maintained constant (about 120 μm). But the penetration length in HAF2₊ increased by nearly 600 μm when P_0 decreased from 2.0 W to 1.5 W.

They supposed that an inner ring area, which was observed around the cavities after fiber fuse propagation, was the trail of glass being melted. D_{melted} defined as the diameter of melting area (see Figure 3) was considered as the radial size of plasma generated in the fiber fuse.

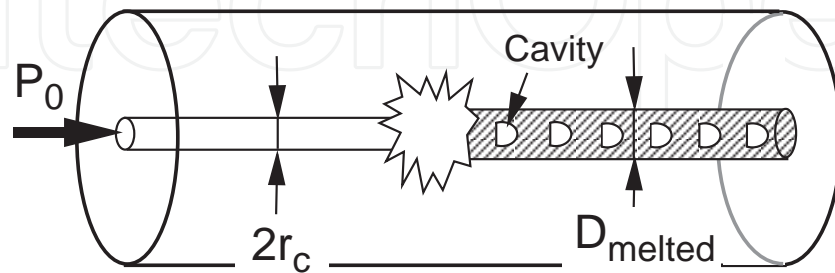


Figure 3. Schematic view of damaged SMF.

D_{melted} of HAF2₊ was maintained constant (about 20–22 μm) in the P_0 range of 2.0–8.1 W, and decreased with decreasing P_0 in the P_0 range of 1.33–2.0 W [42], [47]. The constant D_{melted} value (about 20–22 μm) was almost equal to the D_{hole} value (21.2 μm) of HAF2₊ in the P_0 range of 2.0–8.1 W. Therefore, an increase in penetration length observed in HAF2₊ for $P_0 \leq 2$ W was considered to be induced by the reduction of plasma size. On the other hand, D_{melted} of an SMF increased monotonously with increasing P_0 in the P_0 range of 4–14 W [46].

Several hypotheses have been put forward to explain the fiber fuse phenomenon. These include a chemical reaction involving the exothermal formation of germanium (Ge) defects [18], self-propelled self-focusing [3], thermal lensing of the light in the fiber via a solitary thermal shock wave [5], and the radiative collision of SiO and O complexes [52]–[55].

The similarities between the fiber fuse propagation and the combustion flame propagation were pointed out by Facão *et al.* [56], Todoroki [15], and Ankiewicz [57]. A fast detonation-like mode of fiber fuse propagation with a velocity of 3.2 km/s was observed under intense laser radiation intensity of 4,000 MW/cm² [58]. Combustion processes, including thermal self-ignition, can be mathematically expressed by the reaction-diffusion equations for temperature and fuel concentration [59], [60], [61]. If the reaction term for fuel concentration in these equations is replaced by the heat source term resulting from light absorption, the fiber fuse propagation can be described by solving the equations [56], [57], [62].

The optical absorption coefficient α of a fiber core at high temperatures is closely related to the generation of the fiber fuse. Kashyap reported a remarkable increase in the α value of a Ge-doped silica core above the critical temperature T_0 ($\sim 1,323$ K), while the α value of about 0 dB/km at room temperature remained unchanged until the temperature (T) approached T_0 [4]. The α value increased by nearly 1,900 dB/km ($\sim 0.44 \text{ m}^{-1}$) at $\lambda_0 = 1.064 \mu\text{m}$ when T

changed from T_0 to $T_0 + 50$ K. Furthermore, Kashyap *et al.* reported that the best fit between the experimental and theoretical fiber fuse velocities was obtained when the α value of the Ge-doped silica core at high temperatures of above T_0 was fixed to be $4.0 \times 10^4 \text{ m}^{-1}$ at $1.064 \mu\text{m}$ [19].

Hand and Russell found that this phenomenon was initiated by the generation of large numbers of Ge-related defects at high temperatures of above about 1,273 K, and the α values at $\lambda_0 = 0.5 \mu\text{m}$ obtained at temperatures of below 1873 K were modeled quite accurately using an Arrhenius equation [5], [6]. By contrast, they reported that the best fit between the experimental and theoretical fiber fuse velocities was obtained when the α value of the Ge-doped silica core at 2,293 K was assumed to be $5.6 \times 10^4 \text{ m}^{-1}$ at $0.5 \mu\text{m}$ [5]. This large α value, however, could not be estimated using their Arrhenius equation [6]. As the focal length F of thermal lense effect is inversely as the α value [63], large α value of $5.6 \times 10^4 \text{ m}^{-1}$ is necessary to obtain small F value of $10 \mu\text{m}$ order, which is comparable with observed interval and/or large front size of the cavities (see Appendix).

Furthermore, Hand and Russell reported that the electrical conductivity σ of the fiber core increased with the temperature and that the hot spot at the fiber fuse center was plasmalike [5]. Kashyap considered that the large α values may be attributable to an increase in the σ value of the fiber core at high temperatures of above T_0 [4].

It is well known that silica glass is a good insulator at room temperature, and the electrical conductivity in silica glass below 1,073 K is due to positively charged alkali ions moving under the influence of an applied field [64], [65]. The ionic conduction in the glass is not related solely to optical absorption.

We previously investigated the optical absorption mechanism causing the increase in the σ value and reported the relationship between σ and α in silica glass at high temperatures of above 1,273 K [66]–[69]. It was found that the increase in loss observed at $1.064 \mu\text{m}$ can be well explained by the electronic conductivity induced by the thermal ionization of a Ge-doped silica core, and it is not directly related to the absorption of Ge E' centers.

However, the calculated α values resulting from the electronic conductivity at $1.064 \mu\text{m}$ were of 10^2 m^{-1} order at 2,873 K, about two orders smaller than the α values (1.0 – $4.0 \times 10^4 \text{ m}^{-1}$) reported by Kashyap *et al.* [4], [19]. Therefore, we need another mechanism to explain the increase in loss at high temperatures of above 2,273 K to account for the large (10^4 m^{-1} order) α values.

To satisfy this requirement, we proposed a thermochemical SiO_x production model in 2004 [68], [69]. Using this model, we theoretically estimated large α values of 10^4 m^{-1} order as a result of SiO_x absorption at high temperatures of 2,800 K or above. This model was able to quantitatively explain the relation between the fiber fuse propagation velocity and the incident laser-power intensity previously reported by other research institutions.

On the other hand, since the parameters (particularly the light-absorbing parameter) used for the numerical simulation were not optimized, the shortcoming that the maximum temperature of the core center obtained by calculation became unusually high (10^5 K order) was observed.

We have improved this model by optimizing several parameters required for the numerical computation, and we proposed an improved model in 2014 [70].

In the first half of this chapter we describe the improved model in detail. That is, we explain the mechanism of the increased absorption in optical fibers at high temperatures due to the thermochemical production of SiO_x , and estimate high-temperature α values at $\lambda_0 = 1.064 \mu\text{m}$. Then, using these values, we theoretically study the non-steady-state thermal conduction process in a single-mode optical fiber using the explicit finite-difference technique.

Next we have analyzed the heat transfer of HAFs with $d_h = r_c$ on the basis of the improved model, and simulated the fiber fuse propagation behavior when a high optical power of 1–20 W at $\lambda_0 = 1.55 \mu\text{m}$ is injected into an HAF. In the latter half of this chapter we describe the results of this analysis.

2. High-temperature optical absorption in optical fibers

2.1. Effect of SiO_x formation on absorption

It has been reported that, at elevated temperatures, silica glass is thermally decomposed by the reaction [71]



Among the reductants of the silica generated by this pyrolysis reaction with the formula SiO_x , the most thermally stable material is SiO ($x = 1$).

The internal core space heated at the elevated temperature is shielded from the external conditions. Thus, with increasing temperature, the internal pressure increases and the internal volume decreases. Dianov *et al.* reported that the internal core temperature is about 10,000 K and the internal pressure is about 10,000 atmospheres at the time of fiber fuse evolution [72]. It is thought that SiO_x generated under the high-temperature and high-pressure conditions is densely packed into the internal core space because it is not allowed to expand, and it exists in a liquidlike form. For this reason, it is thought that the optical absorption spectrum of the high-density SiO_x in the core space is similar to that of solid SiO_x .

Philipp reported that the optical absorption spectrum of a SiO_x film is similar to that of amorphous Si because of the many Si–Si bonds in a SiO_x film, and that the absorption coefficient α_{SiO} for SiO ($x = 1$) near the threshold energy should be about one-twentieth of that for amorphous Si α_{Si} [73]. Furthermore, Philipp estimated the theoretical concentration f_{Si} of Si–(Si_4) when the five possible tetrahedral conformations centering on Si, Si–(Si_4), Si–(Si_3O), Si–(Si_2O_2), Si–(SiO_3), and Si–(O_4), were completely distributed at random within amorphous SiO_x [74]. The relationship between f_{Si} and x for SiO_x is illustrated in Figure 4. According to Figure 4, f_{Si} for a SiO ($x = 1$) film is 6.25% ($= 1/16$). This is very close to the factor by which the α value was reduced (about $1/20$) as reported by Philipp [73].

The optical absorption near the absorption edge of a SiO_x film is dominated by that of amorphous Si with the Si–(Si_4) tetrahedral conformation, and the optical absorption coefficient α_{SiO_x} near the absorption edge of a SiO_x film can be calculated by multiplying the value of α_{Si} for amorphous Si by f_{Si} . That is, if the production rate of SiO_x given by Eq.

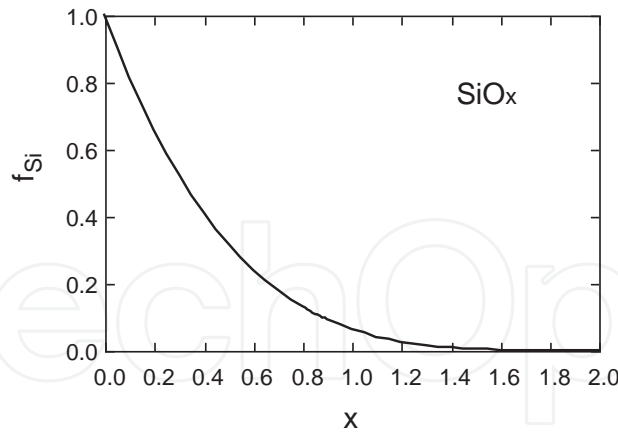


Figure 4. Relative content of Si-(Si₄) in SiO_x.

(1) is denoted by g_{SiO_x} , then α_{SiO_x} at temperature T is given by

$$\alpha_{\text{SiO}_x}(T) = g_{\text{SiO}_x}(T) f_{\text{Si}}(x) \alpha_{\text{Si}}(T). \quad (2)$$

2.2. Production rate of SiO_x

The most thermally stable compound in SiO_x generated via Eq. (1) is SiO ($x = 1$). Therefore, the production rate g_{SiO_x} of SiO_x in Eq. (2) is assumed to be almost equal to the production rate g_{SiO} of SiO.

g_{SiO} at temperature T can be calculated as the ratio of the molar concentration c_{SiO} of SiO at temperature T to the maximum value c_{SiO}^0 . This c_{SiO}^0 is the molar concentration when SiO₂ changes to SiO via Eq. (1) with a yield of about 100%.

We assumed that the pyrolysis reaction system given by Eq. (1) reaches its equilibrium state during fiber fuse propagation. The equilibrium constant for Eq. (1) is denoted as K_c . The value of c_{SiO} at temperature T was calculated using K_c as described below.

First, the initial molar concentration $c_{\text{SiO}_2}^s$ ($= 0.0366 \text{ mol cm}^{-3}$) is denoted by a . We consider the case that the SiO₂ concentration decreases to $a - y$ via the pyrolysis reaction of Eq. (1). In this case, the molar concentration of SiO and the molar concentration c_{O_2} of O₂ are expressed as y and $y/2$, respectively. K_c is given in terms of a and y as follows:

$$K_c = \frac{c_{\text{SiO}} c_{\text{O}_2}^{1/2}}{c_{\text{SiO}_2}} = \frac{y(y/2)^{1/2}}{a - y}. \quad (3)$$

Rearranging Eq. (3), we obtain a cubic equation in y . The solution of this equation is given by

$$y = \sqrt[3]{C} + \frac{4K_c^2}{3\sqrt[3]{C}} \left(\frac{K_c^2}{3} - a \right) + \frac{2K_c^2}{3}, \quad (4)$$

where

$$C = a^2 K_c^2 - \frac{4}{3} a K_c^4 + \frac{8}{27} K_c^6 + a^2 K_c^2 \sqrt{1 - \frac{8 K_c^2}{27 a}} \quad (5)$$

It is well known that the equilibrium constant K_c is related to the standard Gibbs energy change $\Delta_r G^0$ for Eq. (1). The relationship between K_c and $\Delta_r G^0$ is given by [75]

$$\ln K_c = \frac{-\Delta_r G^0}{RT}, \quad (6)$$

where R is the gas constant. The $\Delta_r G^0$ value for Eq. (1) is given by

$$\Delta_r G^0 = \Delta_f G_{\text{SiO}}^0 + (1/2) \Delta_f G_{\text{O}_2}^0 - \Delta_f G_{\text{SiO}_2}^0, \quad (7)$$

where $\Delta_f G^0$ is the standard production Gibbs energy of a reactant and/or a product.

Vitreous silica (SiO_2) is a solid at the standard temperature (298.15 K). It melts at high temperatures of above 1,996 K, and becomes a liquid. It also becomes a vapor at temperatures of above 3,000 K.

The standard production Gibbs energies $\Delta_f G_{\text{SiO}_2}^0$, $\Delta_f G_{\text{SiO}}^0$, and $\Delta_f G_{\text{O}_2}^0$ in each phase have been published [76]. Thus, using these $\Delta_f G^0$ values, we first calculated the standard Gibbs energy change $\Delta_r G^0$ for Eq. (1). Next, we calculated K_c by substituting the $\Delta_r G^0$ value into Eq. (6). In this way, we computed c_{SiO} ($= y$) at temperature T by substituting K_c and a ($= 0.0366 \text{ mol cm}^{-3}$) into Eqs. (4) and (5). The relationship between c_{SiO} and T is shown in Figure 5. c_{SiO} increases with increasing T and gradually approaches its maximum value ($c_{\text{SiO}}^0 \cong 0.0366 \text{ mol cm}^{-3}$) at T of about 3,200 K.

Therefore, g_{SiO_x} at temperature T was estimated by dividing the value of c_{SiO} calculated above by c_{SiO}^0 ($\cong 0.0366 \text{ mol cm}^{-3}$).

2.3. Absorption coefficient of amorphous Si

The optical absorption spectrum of amorphous Si was reported by Brodsky *et al.* [77]. The absorption coefficient α_{Si} of amorphous Si in Eq. (2) was estimated as follows.

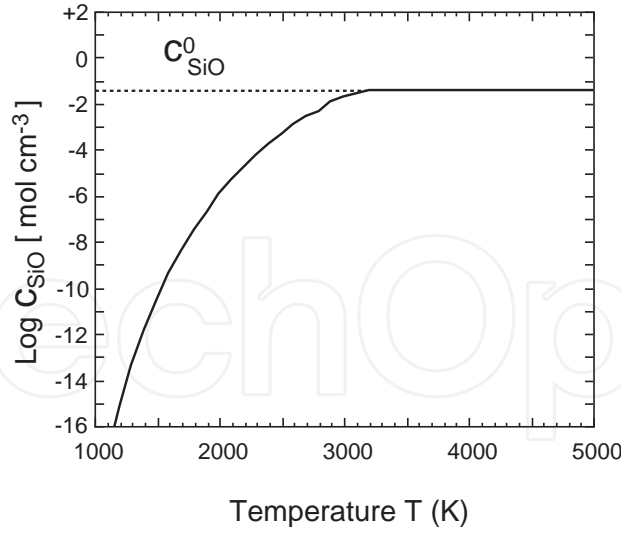


Figure 5. Molar concentration of SiO vs. temperature.

First, we consider the absorption coefficient α_{Si} of an interband transition region, where the photon energy $\hbar\omega$ is larger than the energy gap E_g ($= 1.26$ eV) of amorphous Si. In this case, the values of α_{Si} (cm^{-1} unit) near E_g is given by

$$\alpha_{\text{Si}}(\omega) = B \frac{(\hbar\omega - E_g)^2}{\hbar\omega}, \quad (8)$$

where the parameter B is $5.06 \times 10^5 \text{ cm}^{-1} \text{ eV}^{-1}$. The α_{Si} values calculated by Eq. (8) are in good agreement with the experimental values reported by Brodsky *et al.* [77] for the case of $\hbar\omega > 1.5$ eV.

Next, we consider the values of α_{Si} in the low-energy region, where $\hbar\omega < E_g$. In this region, an absorption edge spectrum is broadened as a result of the interaction between optical phonons and electrons (or excitons). α_{Si} in this region exhibits exponential behavior (referred to as an “exponential tail” or “Urbach tail”) as follows [78]:

$$\alpha_{\text{Si}}(\omega) = \alpha_0 \exp \left[\frac{\gamma(\hbar\omega - E_g)}{kT^*} \right], \quad (9)$$

where α_0 and γ are parameters and k is the Boltzmann constant. T^* is the effective temperature. If the characteristic temperature of phonons is denoted by θ , then T^* is given by [79]

$$T^* = \frac{\theta}{2} \coth \left(\frac{\theta}{2T} \right). \quad (10)$$

For Si, $\theta = 600$ K [80]. α_0 and γ are estimated to be $9.016 \times 10^3 \text{ cm}^{-1}$ and 0.14, respectively, by simulation using the experimental α_{Si} values reported by Brodsky *et al.* [77].

It is known that the energy gap E_g of Si decreases linearly with increasing T at $T > 200$ K [81]. The temperature dependence of E_g (eV unit) at $T > 300$ K is given by

$$E_g = 1.26 - \beta T, \quad (11)$$

where β is the temperature coefficient of the energy gap and takes a value of 4.2×10^{-4} eV/K [82].

2.4. Absorption coefficient of SiO_x

On the basis of the above results, the temperature dependence of α_{SiO_x} at $1.064 \mu\text{m}$ ($\hbar\omega = 1.17$ eV) was calculated using Eq. (2) and the c_{SiO} values shown in Figure 5. $f_{\text{Si}} = 0.0625$ ($x = 1$) was used in the calculation. The results are shown in Figure 6.

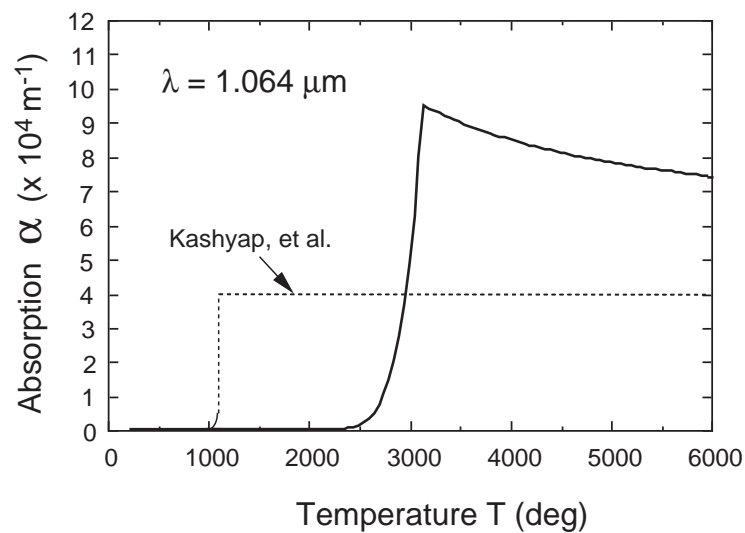


Figure 6. Absorption coefficient of SiO_x at $1.064 \mu\text{m}$ vs. temperature. The thick solid line was calculated using Eq. (2). The dotted line shows the values estimated by Kashyap *et al.*

The α_{SiO_x} values (shown as the thick solid line in Figure 6) are about $1.5 \times 10^4 \text{ m}^{-1}$ at 2,800 K and about $3.5 \times 10^4 \text{ m}^{-1}$ at 2,950 K. These values are close to $4 \times 10^4 \text{ m}^{-1}$ (shown as the dotted line in Figure 6), which was estimated by simulation using the finite element method [19].

Moreover, it turns out that α_{SiO_x} reaches its maximum value (about $9.47 \times 10^4 \text{ m}^{-1}$) at about 3,150 K, then decreases gradually with increasing temperature.

Compared with the stepwise shape (dotted line in Figure 6) of the absorption coefficient assumed by Kashyap *et al.*, the maximum value (about $9.47 \times 10^4 \text{ m}^{-1}$) of α_{SiO_x} is about 2.4 times the assumed value ($4 \times 10^4 \text{ m}^{-1}$), and the graph has the shape of a somewhat distorted echelon form.

As mentioned above, SiO_x is produced in the pyrolysis of vitreous silica, and it induces a very large amount of optical absorption with a large absorption coefficient of 10^4 m^{-1} order at

high temperatures of above 2,800 K. It is thought that the large amount of optical absorption at high temperatures is the cause of the genesis of the fiber fuse phenomenon.

We investigated the thermal conduction behavior within an SMF by numerical computation using the thermochemical SiO_x production model. In the next section, we describe the results of some numerical calculations related to the thermal conduction process in an SMF.

3. Simulation of fiber fuse in SMF

3.1. Heat conduction in SMF

We assume the SMF to have a radius of r_f and to be in an atmosphere with temperature $T = T_a$. We also assume that part of the core layer of length ΔL is heated to a temperature of $T_c^0 (> T_a)$ (see Figure 7). Such a region, called the “hot zone” in Figure 7, can be generated by heating the fiber end faces using the arc discharge of a fusion splice machine.

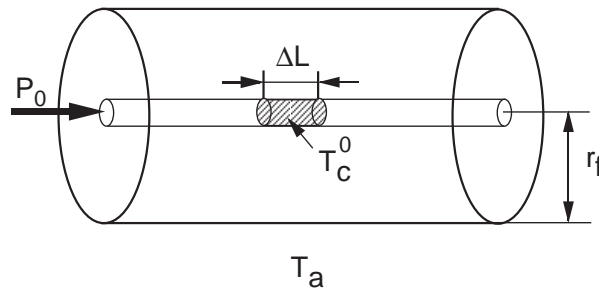


Figure 7. Hot zone in the core layer.

As explained above, the optical absorption coefficient α of the core layer in an optical fiber is a function of temperature T , and α increases with increasing T . In the hot zone in Figure 7, the α values are larger than those in the remainder of the core region because of its elevated temperature. Thus, as light propagates along the positive direction (away from the light source) in this zone, considerable heat is produced by light absorption.

In the case of a heat source in part of the core layer, the nonsteady heat conduction equation for the temperature field $T(r, z, t)$ in the SMF is given by [83]

$$\rho C_p \frac{\partial T}{\partial t} = \lambda \left(\frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} \right) + \dot{Q}, \quad (12)$$

where ρ , C_p , and λ are the density, specific heat, and thermal conductivity of the fiber, respectively. The values of ρ , C_p , and λ used for the calculation are described in the next subsection.

The last term \dot{Q} in Eq. (12) represents the heat source resulting from light absorption, which is only required for the hot zone in the fiber core. \dot{Q} can be expressed by

$$\dot{Q} = \alpha I, \quad (13)$$

where I is the optical power intensity in the core layer, which can be estimated by dividing the incident optical power P by the effective area A_{eff} of the fiber.

3.2. Heat conduction parameters

In the heat conduction calculation for SMFs, we used the following values of λ ($\text{W m}^{-1} \text{K}^{-1}$), ρ (kg m^{-3}), and C_p ($\text{J kg}^{-1} \text{K}^{-1}$) in each temperature range. The unit of T is K (Kelvin).

(1) Parameters in the temperature range from room temperature (298 K) to 1,996 K [84]:

$$\begin{aligned} C_p &= 1194.564 + 31.541 \times 10^{-3}T \\ &\quad - 651.396 \times 10^{-5}T^{-2} \\ \lambda &= 9.2 \\ \rho &= 2,200.0. \end{aligned}$$

(2) Parameters in the temperature range from 1,996 to 3,000 K [84]:

$$\begin{aligned} C_p &= 1,430.490 \\ \lambda &= 9.2 \\ \rho &= 2,200.0. \end{aligned}$$

(3) Parameters for $T > 3,000$ K:

$$\begin{aligned} C_p &= 844.4 \\ \lambda &= 0.0025247\sqrt{T} \\ &\quad + 1.84275 \times 10^{-13}T^{5/2} \\ \rho &= 2,024.0. \end{aligned}$$

In (3), the first term in the expression for λ was estimated by substituting the parameters for SiO in the following equation, which represents the thermal conductivity of diatomic molecules derived from the kinetic theory of gases [85]:

$$\lambda = \frac{5}{3\sigma^2} \sqrt{\left(\frac{k}{\pi}\right)^3 \frac{N_A}{M}} \sqrt{T}, \quad (14)$$

where N_A is Avogadro's number, M (=44.0854) is the molecular weight of SiO, and σ (= 1.5 Å) is half of the collision diameter.

Moreover, in (3), the second term in the expression for λ was estimated by multiplying the following thermal conductivity equation for weakly ionized gas plasma [86] by the correction factor of 1/20:

$$\lambda = \frac{5N_e k^2 T}{2m_e \nu_c}, \quad (15)$$

where m_e is the electron mass, N_e is the number density of electrons in the plasma, and ν_c is the collision frequency. If we assume that electrons mainly collide with ions with a charge of +1 in the plasma, then ν_c is given by [87]

$$\nu_c = \sqrt{\frac{2}{9\pi}} \frac{N_e e^4}{\epsilon_0^2 m_{fe}^2} \left(\frac{m_e}{3kT} \right)^{3/2} \ln \Lambda, \quad (16)$$

where e is the electron charge and ϵ_0 is the permittivity of free space. $\ln \Lambda$ is the so-called Coulomb logarithm, and it takes values of 4–34 in the electron temperature range of 10^2 – 10^8 K and the N_e range of 1 – 10^{24} cm^{-3} [88]. In our calculation, we used $\ln \Lambda = 16.155$, which corresponds to the case of $T \sim 10^4$ K and $N_e \sim 10^6$ cm^{-3} .

3.3. Boundary and initial conditions for heat conduction

We solved Eq. (12) using the explicit finite-difference method (FDM) [89] under the boundary and initial conditions described below.

The area in the numerical calculation had a length of $2L$ ($= 4$ cm) in the axial (z) direction and a width of $2r_f$ ($= 125$ μm) in the radial (r) direction. There were 24 and 2,000 divisions in the r and z directions, respectively, and we set the calculation time interval to 1 μs . We assumed that the hot zone was located at the center of the fiber (length $2L$) and that the length ΔL of the hot zone was 40 μm .

The boundary conditions are as follows:

(1) Since the temperature distribution of the optical fiber is axisymmetric, the amount of heat conducted per unit area (heat flux) in the r direction is set to 0 at the fiber center ($r = 0$) as follows:

$$-\lambda \frac{\partial T}{\partial r} \Big|_{r=0} = 0. \quad (17)$$

(2) At the outer fiber surface ($r = r_f$), the amount of heat conducted per unit area (heat flux) is dissipated by radiative transfer or heat transfer to the open air and/or the jacketing layer ($T = T_a$) as follows:

$$\begin{aligned} -\lambda \frac{\partial T}{\partial r} \Big|_{r=r_f} &= \sigma_S \epsilon_e (T^4 - T_a^4) \\ &+ \frac{\lambda}{\delta r_t} (T - T_a), \end{aligned} \quad (18)$$

where σ_S is the Stefan-Boltzmann constant and ϵ_e (~ 0.9) is the emissivity of the surface. δr_t is the thickness of the thermal boundary layer and $\delta r_t = \delta r$ is assumed in our calculation, where δr is the step size along the r axis.

(3) At the center ($z = 0$) of the hot zone, the temperature of the fiber core center is T_c^0 . Also, there is heat inflow along the z axis only at the core center ($r = 0$), which is attributable to light absorption. Moreover, when $r \neq 0$ and $z = 0$, there is neither heat inflow nor heat outflow along the z axis. These conditions are given by

$$-\lambda \left. \frac{\partial T}{\partial z} \right|_{z=0} = \begin{cases} \alpha I, & \text{if } r = 0 \\ 0 & \text{if } r \neq 0. \end{cases} \quad (19)$$

(4) At both fiber ends ($z = \pm L$), the amount of heat conducted per unit area (heat flux) is dissipated by radiation transfer to the open air ($T = T_a$) as follows:

$$-\lambda \left. \frac{\partial T}{\partial z} \right|_{z=\pm L} = \sigma_S \epsilon_e (T^4 - T_a^4). \quad (20)$$

In contrast, as initial conditions, $T = T_a$ in the optical fiber at $t = 0$, except in the hot zone, and the core-center temperature in the hot zone is equal to $T_c^0 (> T_a)$ as follows:

$$T(0, z, 0) = \begin{cases} T_a, & \text{if } -L \leq z < -\Delta L/2 \\ T_c^0, & \text{if } -\Delta L/2 \leq z \leq \Delta L/2 \\ T_a & \text{if } \Delta L/2 < z \leq L. \end{cases} \quad (21)$$

When light propagates through the fiber core ($r = 0$) along the z direction (away from the light source), the incident laser power P decreases because of the nonzero optical absorption coefficient α . When the laser light propagates from z to $z + \delta z$ along the z axis at $r = 0$, the P value is given by

$$P = P_0 \exp \left(-\alpha \delta z - \int_{-L}^z \alpha(T) dz \right), \quad (22)$$

where P_0 is the initial laser power. The second term on the right-hand side expresses the optical absorption loss when the light propagates through a distance of $z - L$.

The results described above assume that the laser light propagates through the fiber core along the positive z direction (away from the light source).

When the core layer is heated to above the vaporization point of silica (~ 3273 K), an enclosed hollow cavity is produced in the core center. This cavity contains oxygen, which is produced by the pyrolysis reaction of Eq. (1). The heat conductivity κ of the oxygen ($0.03 \text{ W m}^{-1} \text{ K}^{-1}$) is two orders smaller than that of the silicate glass. Therefore, the heat transferred in the silica core is stopped at the cavity.

Moreover, as the cavity has a refractive index of $n \sim 1$, which is smaller than that of the silica core ($n_1 = 1.46$), the light propagating in the core layer is reflected at the cavity wall. When the light direction is reversed at the cavity, the heat source term αI_r resulting from the optical absorption of the reflected light is added to αI in Eq. (13), where I_r is the optical power intensity of the reflected laser light.

We consider the P value at a z position located near the cavity wall. The length of this position is assumed to be δz . The laser light reaches z , propagates through a distance of δz , and then reaches the cavity wall, whose coordinate is z_v . Next, the light is reflected at the cavity wall and propagates in the negative z direction, and then reaches z again. In such a case, the P value at z is given by

$$P = P_0 \exp \left(-\alpha \delta z - \int_{-L}^z \alpha(T) dz \right) \times R \exp \left(-2 \int_{z+\delta z}^{z_v} \alpha(T) dz \right), \quad (23)$$

where R is the reflectivity at the boundary of the silica core and the cavity. R is given by

$$R = \left(\frac{n_1 - 1}{n_1 + 1} \right)^2. \quad (24)$$

The second integral on the right-hand side of Eq. (23), which is related to the reflected light, slightly affects the occurrence of the fiber fuse. However, by taking this term into consideration, the calculated fiber fuse velocities fit the experimental values. For this reason, in the present work, we decided to take into account the effect of the reflected light.

In the following section, we describe the calculated time (t) dependence of $T(r, z)$ in an SMF.

3.4. Propagation of fiber fuse in SMF

In the calculation, we used $T_c^0 = 2923$ K and $T_a = 298$ K. It was assumed that laser light of wavelength $\lambda_0 = 1.064$ μm and $P_0 = 2$ W was incident to an SMF-28 optical fiber, which has a core diameter of $2r_c = 8.2$ μm , a refractive index difference of $\Delta = 0.36\%$, and $A_{eff} = 49.4091 \times 10^{-12}$ m^2 .

We calculated the $T(r, z)$ values at $t = 1, 11$, and 21 ms after the incidence of the 2 W laser light. The calculated results are shown in Figures 8 ~ 10, respectively.

As shown in Figure 8, the core center temperature near the end of the hot zone ($z = -0.7$ mm) changes abruptly to a large value of about 3.4×10^4 K after 1 ms. This rapid rise in the temperature initiates the fiber fuse phenomenon as shown in Figures 9 and 10. After 11 and 21 ms, the high-temperature front in the core layer reached z values of -6.1 and -11.5 mm, respectively. The average propagation velocity v_f was estimated to be 0.54 m/s using these data.

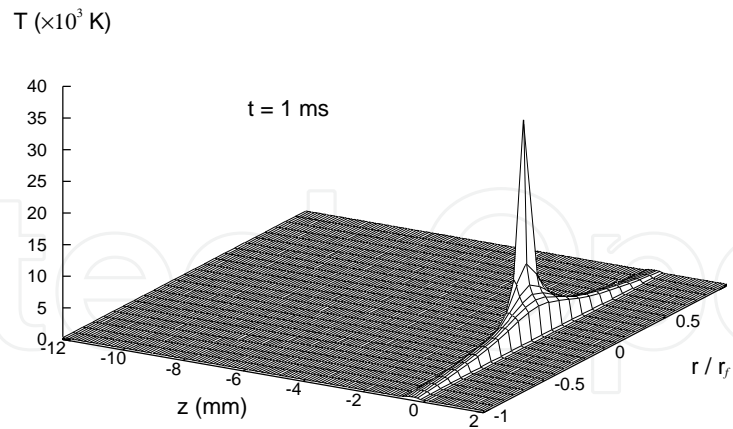


Figure 8. Temperature field in SMF-28 after 1 ms when $P_0 = 2$ W at $\lambda_0 = 1.064$ μm .

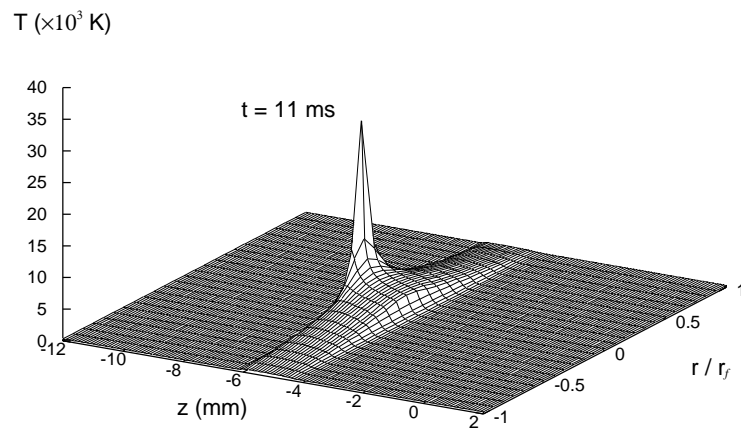


Figure 9. Temperature field in SMF-28 after 11 ms when $P_0 = 2$ W at $\lambda_0 = 1.064$ μm .

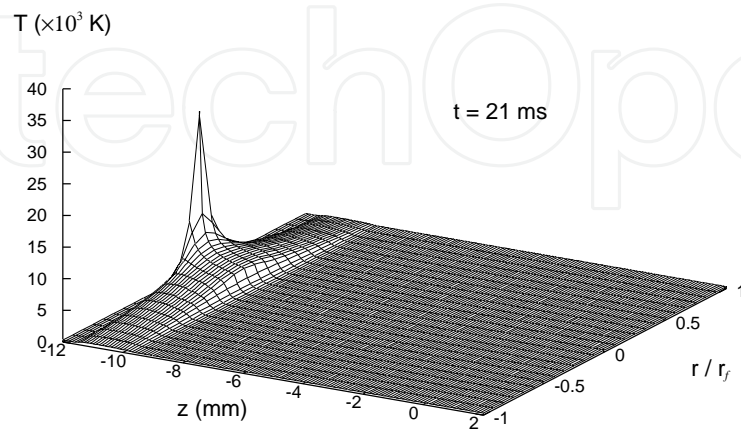


Figure 10. Temperature field in SMF-28 after 21 ms when $P_0 = 2$ W at $\lambda_0 = 1.064$ μm .

When the laser light of $\lambda_0 = 1.064 \mu\text{m}$ and $P_0 = 2 \text{ W}$ is incident to the SMF-28 optical fiber, the optical power intensity is $I = 4.048 \text{ MW/cm}^2$. The fiber fuse velocity at this value of I is estimated to be about 0.55 m/s (see Figure 10 in [69]). This value is in very good agreement with the upper value obtained by calculation (0.54 m/s).

On the other hand, Hand and Russell measured the fiber fuse temperature to be $5,400 \text{ K}$ [5], and Dianov *et al.* obtained a temperature of $4,700\text{--}10,500 \text{ K}$ [28],[90] by measurement. They estimated the temperatures from precisely measured spectral data in the $600\text{--}1,400 \text{ nm}$ [5] and $500\text{--}800 \text{ nm}$ [28],[90] regions, while assuming blackbody radiation.

In our calculation, the temperature distribution of the fiber fuse in the core center is shown in Figure 11. Similar shapes of temperature distribution were reported by Kashyap *et al.* [19]

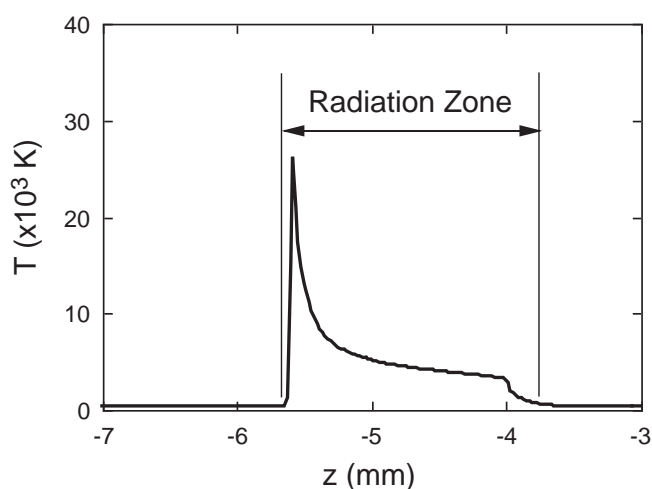


Figure 11. Temperature distribution of the SMF-28 core center vs. length along the z direction when $P_0 = 2 \text{ W}$ at $\lambda_0 = 1.064 \mu\text{m}$. The time after the laser incidence is 10 ms .

and Facão *et al.* [56].

As shown in Figure 11, it is clear that the sharp temperature peak is located near the light source, and a relatively high temperature plateau of about $5,000 \text{ K}$ extends over about 1.5 mm behind the sharp peak. This region, called the “radiation zone” in Figure 11, exhibits high temperatures of above 323 K .

When gaseous SiO and/or SiO_2 molecules are heated to high temperatures above $5,000 \text{ K}$, they decompose to form Si and O atoms, and finally becomes Si^+ and O^+ ions and electrons in the ionized gas plasma state [91]. The numbers of electrons and ions in the plasma front, which exhibits sharp temperature peak, are larger than those in the plateau region. However, as the plasma tends to restore electrical neutrality, the motions of the electrons and ions will not produce any change on the initial temperature distribution shown in Figure 11, except for the peak temperature reduction of the plasma front due to energy loss induced by electron-ion collisions.

In the ionized gas plasma, electron-ion collisions generate electromagnetic radiation because of the deceleration during the collisions. This bremsstrahlung emission [92], [93] is a universal and irreducible process of energy loss. If we assume that electrons mainly collide

with ions with a charge of +1 in the plasma, the spectral radiance function I_p for the bremsstrahlung emission is given by [94]

$$I_p = \frac{N_e^2 \nu^2}{\sqrt{T} c^2} \exp\left(-\frac{h\nu}{kT}\right), \quad (25)$$

where N_e is the number density of electrons in the plasma, h is Planck's constant, and ν is the optical frequency. This function is directly proportionate to ν^2 in the case of $h\nu \ll kT$.

On the other hand, in the case of $h\nu \ll kT$, the spectral radiance function I_b for blackbody radiation is given by [95]

$$I_b = \frac{2\pi\nu^2}{c^2} kT. \quad (26)$$

This is well-known as the Rayleigh-Jeans formula, and this function is proportional to ν^2 , too. Therefore, we assumed that the radiation zone, in which the bremsstrahlung emission of the plasma is liberated, can be treated as a blackbody because of its similar dependence on ν .

If we consider the radiation zone as a blackbody, that is isolated from the surrounding nonheated regions, it is expected that the radiation zone will exhibit a radiation spectrum with a broad range of optical frequencies ranging from ultraviolet to infrared. The blackbody temperature T_b of the zone is related to the frequency ν_m of the spectral peak as follows [95]:

$$\nu_m = \frac{2.82kT_b}{h}. \quad (27)$$

If T_{av} is defined as the average temperature of the radiation zone, the T_b will be close to the T_{av} .

The relationship between the T_{av} value and the time after fiber fuse generation is shown in Figure 12. T_{av} exceeds 10000 K immediately after fiber fuse generation but is less than 7000 K after 4 ms. Then it gradually approaches about 5,700 K. The value of 5,760 K shown in Figure 12 is the average T_{av} value from 4 to 30 ms. This temperature (5,760 K) is close to the reported temperatures of 5,400 K [5] and about 5,800 K [90].

Thus, it was found that if a fiber fuse, which exhibits a sharp temperature peak located near the light source, is approximated as a blackbody isolated from the surrounding nonheated regions, its average temperature from 4 ms after the generation of the fiber fuse approaches the experimentally estimated radiation temperatures.

4. Modeling of Hole-Assisted Fiber

In a Hole-Assisted Fiber (HAF), some holes exist around the main core as shown in Figure 1. In this HAF, the minimum distance of the holes from the main core is only $(D_{hole} - 2r_c)/2$. These holes are filled with air at the same temperature as the surrounding air (T_a). Therefore, at the inner surfaces of the holes, it can be expected that heat transfer or radiative transfer

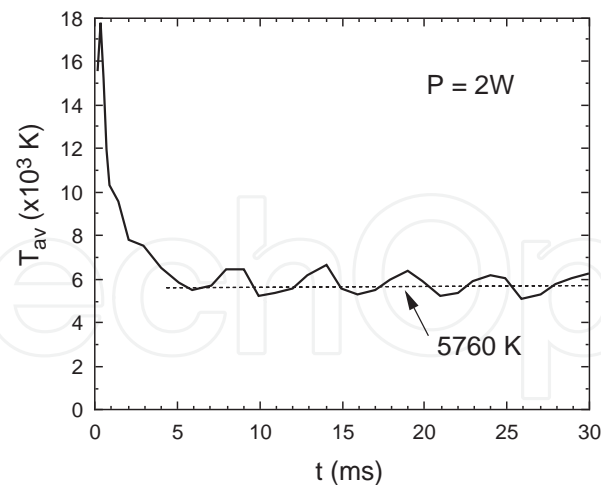


Figure 12. Average temperature of radiation zone vs. time after fiber fuse generation.

will occur between the heated solid inner surfaces of the holes and the gaseous fluid (air) with the low temperature of $T = T_a$. This is expected to affect the heat conduction behavior in the core center of the HAF.

Thus, we used the model proposed by Takara *et al.* [44] for heat conduction analysis, which includes heat transfer or radiative transfer between the inner surfaces of the holes and the gaseous air in the HAF. The proposed model for the HAF is shown in Figure 13.

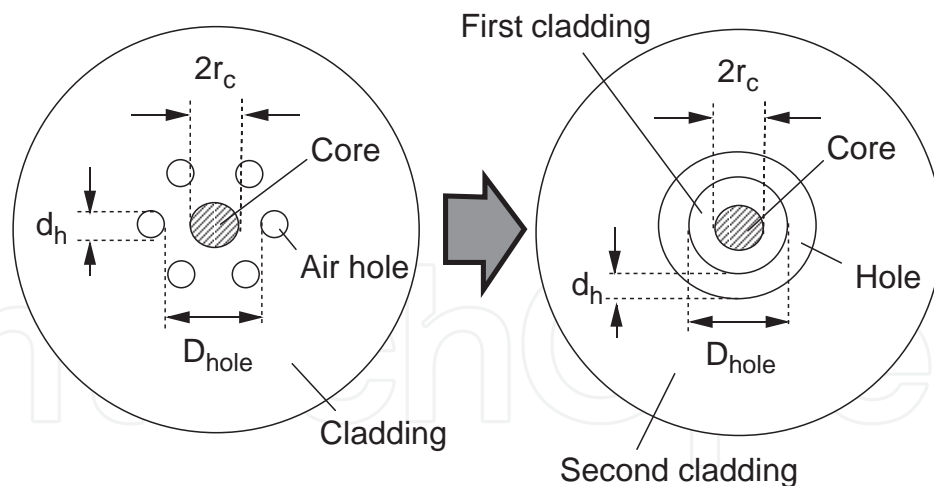


Figure 13. Heat conduction model of HAF [44].

Although bridges of silica glass exist between the holes in an actual HAF, to simplify the calculation, the first cladding layer was assumed to be a cylindrical layer of D_{hole} diameter, and the hole layer was treated as a gap of d_h width, which was inserted between the first and second cladding layers (see Figure 13). The hole layer was assumed to be fulfilled with a silica-air mixture. In the hole layer, the volume ratio of a silica glass to an air was $(1 - \gamma) : \gamma$, where γ_1 is the occupancy of the 6-air holes in the cross section of HAF. Furthermore,

it was assumed that heat transfer and radiative transfer occurred at the inner surface of the hole layer in addition to heat conduction between the silica glass and the silica-air mixture.

When a certain quantity of heat per unit area (heat flux) is conducted from the heated core center to the end of the first cladding layer ($r = D_{hole}/2$) of an optical fiber, a considerable amount of the heat flux is transmitted through the hole layer, and the residual heat flux stagnates in the first cladding layer because the thermal conductivity κ of the hole layer is lower than that of silica glass.

This heat flux stagnating in the first cladding layer can be dissipated by radiative transfer and heat transfer between the outer surface of the first cladding layer and the air in the hole layer with a temperature of T_a .

It is noteworthy here that the total surface area of the 6-air holes existing in an actual HAF is larger than the outer surface area of the first cladding layer when $R_h = 2$ (see Table 1).

The heat transfer results from the convection of air, which is generated by warming the air near the outer surface of the first cladding layer. In this heat transfer, there is a region (called the "thermal boundary layer") near the surface of the first cladding layer where the temperature of the air changes rapidly from a high value to T_a .

5. Heat conduction modeling of HAF

We assume the HAF to have a radius of r_f and to be in an atmosphere with temperature $T = T_a$. We also assume that part of the core layer of ΔL length is heated to a temperature of $T_c^0 (> T_a)$ (see Figure 14).

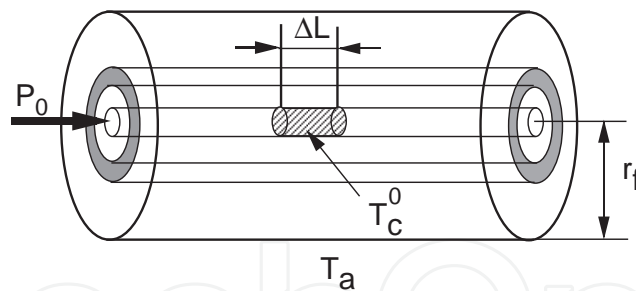


Figure 14. Hot zone in core layer of HAF.

The optical absorption coefficient α of the core layer in a HAF is a function of temperature (T), and it increases with increasing T [70]. In the heating zone (called the "hot zone") shown in Figure 14, α is larger than in other parts of the core because of its high temperature $T_c^0 (> T_a)$. Thus, as light propagates along the positive direction (away from the light source) in this zone, considerable amount of heat is produced by light absorption.

In the case of a heat source in part of the core layer, the nonsteady heat conduction equation for the temperature field $T(r, z, t)$ in the HAF is given by Eq. (12). We can solve Eq. (12) using the explicit finite-difference method (FDM) under the boundary and initial conditions, described in section 3.3, and the additional boundary conditions as follows:

(1) At the outer surface ($r = D_{hole}/2$) of the first cladding layer, the amount of heat conducted per unit area (heat flux) is dissipated by radiative transfer or heat transfer to the air ($T = T_a$) in the hole layer as follows:

$$-\lambda \frac{\partial T}{\partial r} \Big|_{r=D_{hole}/2} = \gamma_1 \sigma_S \epsilon_e (T^4 - T_a^4) + \gamma_1 \frac{\lambda}{\delta r_t} (T - T_a), \quad (28)$$

where γ_1 is the ratio of the total surface area of the 6-air holes existing in an actual HAF to the outer surface area of the first cladding layer, δr_t is the thickness of the thermal boundary layer, and $\delta r_t = x \delta r$ is assumed in the HAF calculation, where $x = 0.5$.

(2) At the inner surface ($r = D_{hole}/2 + d_h$) of the second cladding layer, the amount of heat conducted per unit area (heat flux) is dissipated by radiative transfer or heat transfer to the air ($T = T_a$) in the hole layer as follows:

$$-\lambda \frac{\partial T}{\partial r} \Big|_{r=D_{hole}/2+d_h} = \gamma_2 \sigma_S \epsilon_e (T^4 - T_a^4) + \gamma_2 \frac{\lambda}{\delta r_t} (T - T_a), \quad (29)$$

where γ_2 is the ratio of the total surface area of the 6-air holes existing in an actual HAF to the inner surface area of the second cladding layer.

The fiber parameters of the HAFs used for calculation were $d_h = r_c = 4.5 \mu\text{m}$, which were used in the experiments reported by Hanzawa *et al.* [45]. R_h was set to 2, 3, and 4. In the following, HAFs with $R_h = 2, 3$, and 4 are called HAF2, HAF3, and HAF4, respectively.

The parameters $\gamma, \gamma_1, \gamma_2$ for HAF2, HAF3, HAF4 are shown in Table 1.

Type	γ	γ_1	γ_2
HAF2	0.300	1.50	1.00
HAF3	0.214	1.00	0.75
HAF4	0.167	0.75	0.60

Table 1. Parameters for HAFs.

The area in the numerical calculation has a length of $2L (= 4 \text{ cm})$ in the axial (z) direction and a width of $2r_f (= 125 \mu\text{m})$ in the radial (r) direction. There were 28 and 2,000 divisions in the r and z directions, respectively, and we set the calculation time interval to $1 \mu\text{s}$. We assume that the hot zone is located at the center of the fiber (length $2L$) and that the length ΔL of the hot zone is $40 \mu\text{m}$.

6. Simulation of fiber fuse in HAF

On the basis of the model described above, we calculated the generation and propagation behavior of a fiber fuse in HAFs with $d_h = r_c = 4.5 \mu\text{m}$ using the FDM.

For reference, we also carried out the calculation for an SMF which has $r_c = 4.5 \mu\text{m}$, a refractive index difference $\Delta = 0.3\%$, and $A_{eff} = 98.1318 \times 10^{-12} \text{ m}^2$.

The calculation using the FDM was conducted in accordance with the procedure in [70]. In the calculation, we set the time interval δt to $1 \mu\text{s}$, the step size along the r axis δr to $r_f/14$, the step size along the z axis δz to $20 \mu\text{m}$, respectively, and assumed that $T_c^0 = 2,923 \text{ K}$ and $T_a = 298 \text{ K}$.

We estimated the temperature field $T(r, z)$ of HAFs and/or SMF at $t = 10 \text{ ms}$ after the incidence of laser light with wavelength $\lambda_0 = 1.55 \mu\text{m}$ and an initial power P_0 of 4 W . The calculation results for HAF2, HAF3, and HAF4 are shown in Figures 15–17, respectively, and the result for the SMF is shown in Figure 18.

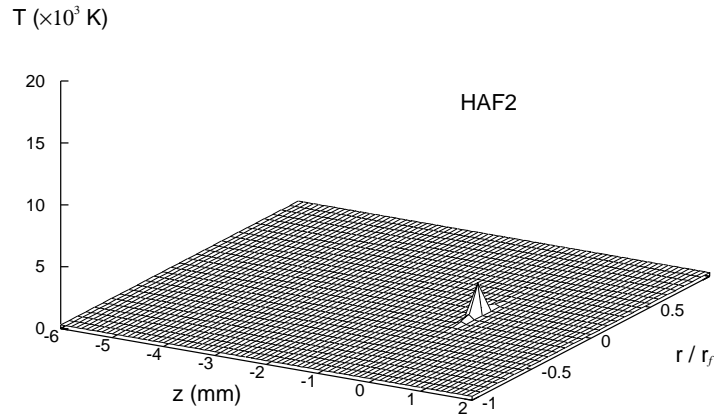


Figure 15. Temperature field in HAF2 after 10 ms after when $P_0 = 4 \text{ W}$ at $\lambda_0 = 1.55 \mu\text{m}$.

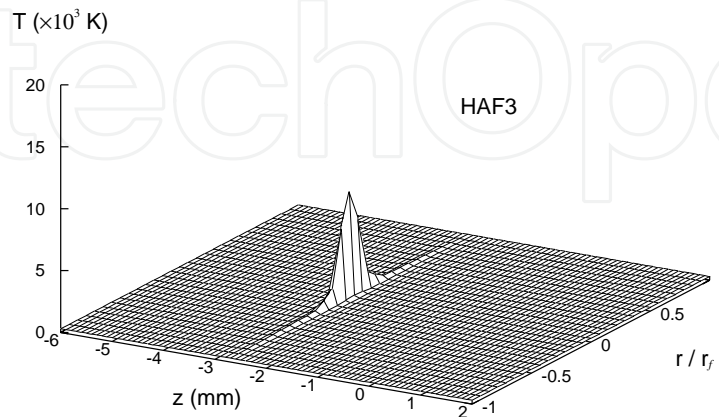


Figure 16. Temperature field in HAF3 after 10 ms when $P_0 = 4 \text{ W}$ at $\lambda_0 = 1.55 \mu\text{m}$.

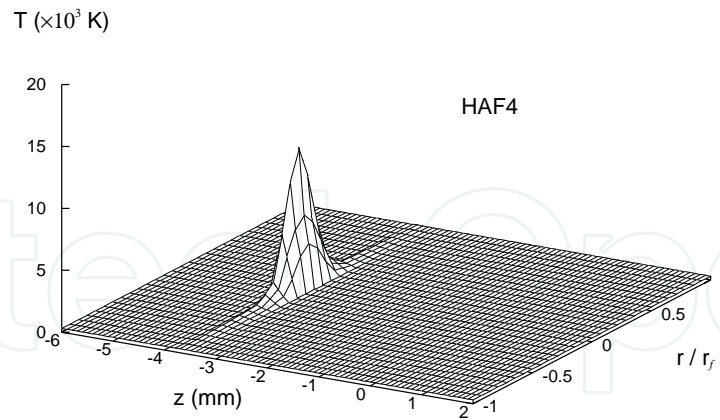


Figure 17. Temperature field in HAF4 after 10 ms when $P_0 = 4$ W at $\lambda_0 = 1.55$ μm .

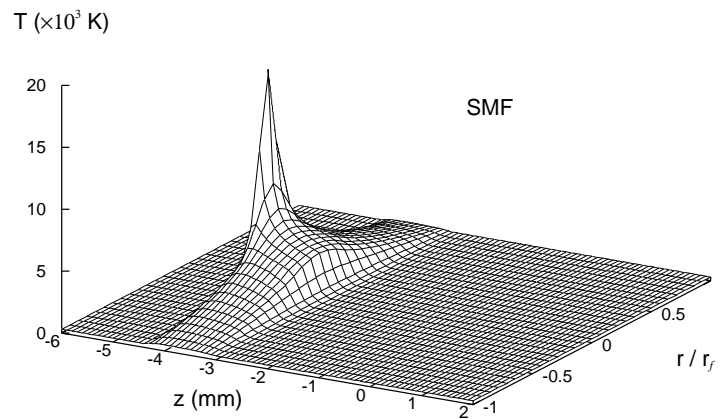


Figure 18. Temperature field in SMF after 10 ms when $P_0 = 4$ W at $\lambda_0 = 1.55$ μm .

As shown in Figures 15–18, the core center temperature at the thermal peak position of HAF2, HAF3, HAF4, and SMF are 2,923 K, 8,756 K, 11,603 K, and 17,528 K, respectively. The rapid rise in the temperature shown in HAF3, HAF4, and SMF initiates the fiber fuse phenomenon. In SMF, the propagation velocity v_f of the fiber fuse was estimated to about 0.43 m/s from the peak shift distance (4.3 mm) per 10 ms of the core center temperature shown in Figure 18. In HAF3 and HAF4, the propagation velocities of the fiber fuse were estimated to about 0.26 and 0.36 m/s, respectively, by using the same procedure as above.

On the other hand, in HAF2, there is no temperature increase in the core layer, as shown in Figure 15, and it means that a fiber fuse was not generated when $P_0 = 4$ W.

We investigated the temperature field $T(r, 0)$ at the end ($z = 0$ mm) of the hot zone in HAF2 after 10 ms when $P_0 = 4$ –10 W at $\lambda_0 = 1.55$ μm . The calculated temperature fields are shown in Figure 19.

When the power of the light entering HAF2 increases from 4 W to 5 W, a thermal wave with a peak temperature of higher than 60,000 K was generated at the end of the hot zone, as

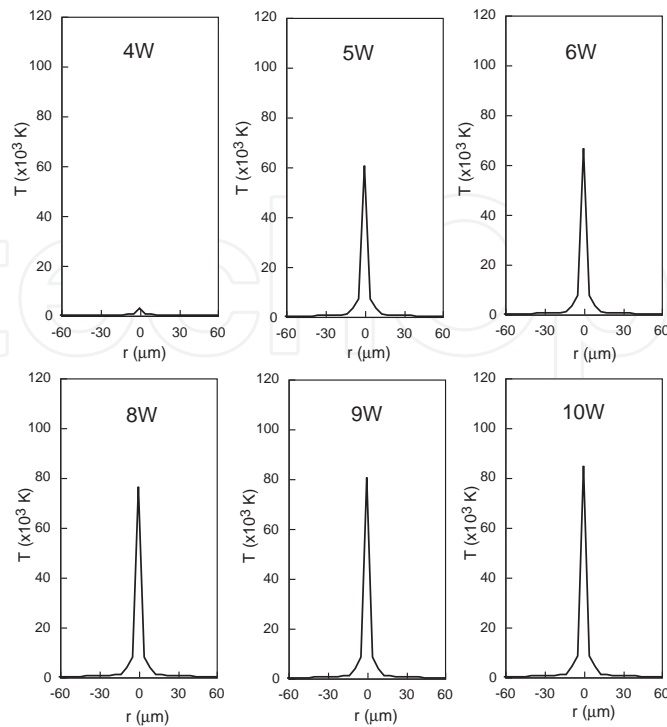


Figure 19. Temperature field at the end of the hot zone in HAF2 after 10 ms when $P_0 = 4\text{--}10$ W at $\lambda_0 = 1.55$ μm .

shown in Figure 19. Figure 20 shows the peak temperature change at the core center ($r = 0$ μm) with passage of time after the incidence of laser light with $P_0 = 5$ W at $\lambda_0 = 1.55$ μm .

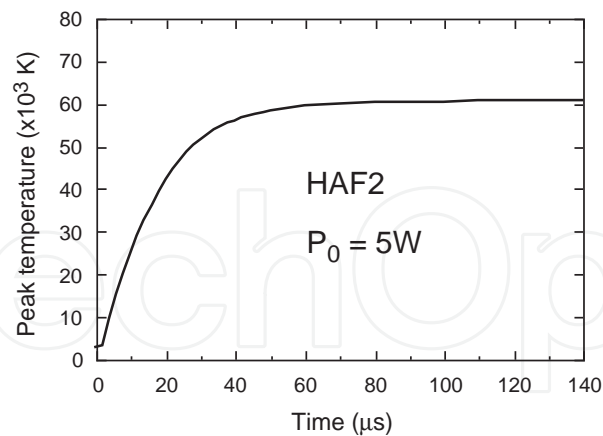


Figure 20. Peak temperature at the core center vs. time after the incidence of laser light with $P_0 = 5$ W at $\lambda_0 = 1.55$ μm .

The core center temperature at the end of the hot zone ($z = 0$ mm) changes abruptly to a large value of $\geq 50,000$ K after 28 μs .

Although a thermal wave with a peak temperature of higher than 60,000 K was generated at the end of the hot zone, it was found that this thermal wave did not increase in size or

propagate in the negative z direction when P_0 increased from 5 W to 10 W, as shown in Figure 19. Such a “stationary” thermal wave was reported by Kashyap [14].

If P_0 is further increased to 11 W and above, the thermal wave increases in size and propagates in the negative z direction toward the light source, as shown in Figure 21.

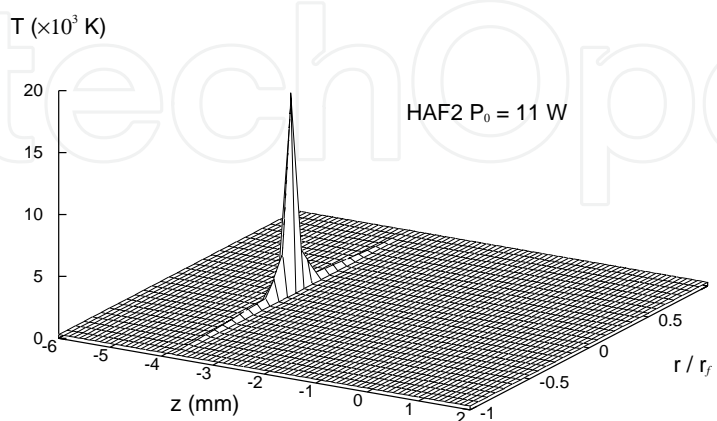


Figure 21. Temperature field in HAF2 after 10 ms after when $P_0 = 11$ W at $\lambda_0 = 1.55 \mu\text{m}$.

When $P_0 = 11$ W, the propagation velocities of the fiber fuse were estimated to about 0.38 m/s by using the same procedure as above.

We calculated the power intensity dependence of the propagation velocity v_p for each HAF and the SMF at $\lambda_0 = 1.55 \mu\text{m}$. The calculation results for the SMF, HAF2, HAF3, and HAF4 are shown in Figure 22.

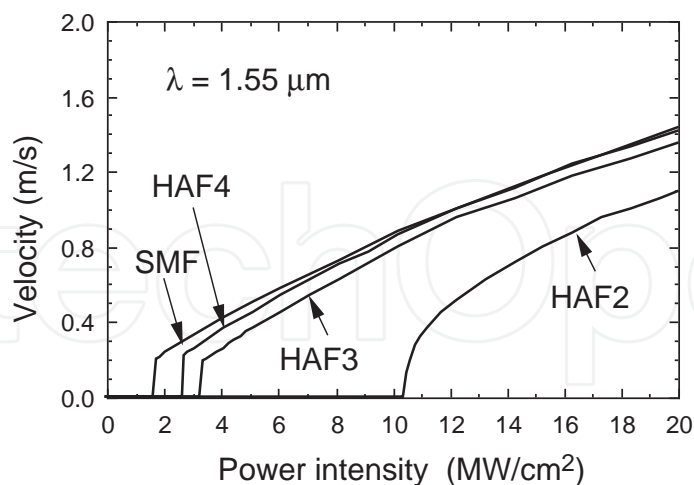


Figure 22. Power intensity vs fiber-fuse propagation velocity for SMF, HAF2, HAF3, and HAF4.

It is clear that the propagation velocity of the HAF4 and/or HAF3 approaches that of the SMF with increasing power intensity.

The threshold power intensity I_{th} for HAF2, HAF3, HAF4, and SMF are shown in Table 2.

Type	I_{th} (MW/cm ²)
HAF2	10.41
HAF3	3.27
HAF4	2.65
SMF	1.63

Table 2. Threshold power intensity for HAFs and SMF.

On the other hand, in HAF2, fiber fuse propagation begins at a threshold power intensity I_{th} of about 10.4 MW/cm² ($P_0 = 10.2$ W), which is much higher than that in HAF3 (about 3.3 MW/cm²) or HAF4 (about 2.7 MW/cm²), as shown in Table 2. The I_{th} of HAF2 is six times that of SMF.

When laser light enters the hot zone of the core layer, heat is produced in the zone by optical absorption of the incident light. In HAF2, the heat generated by optical absorption is effectively dissipated by the heat transfer and radiative transfer between the inner surfaces of the hole layer and the gaseous air. The dissipation of heat in HAF2 is more effective than that in HAF3 or HAF4 because the first cladding layer in HAF2 is thinner than that in HAF3 or HAF4.

Figure 23 shows a schematic view of the relationship between P_0 and the accumulated heat in the hot zone of the core layer for HAF2 and SMF.

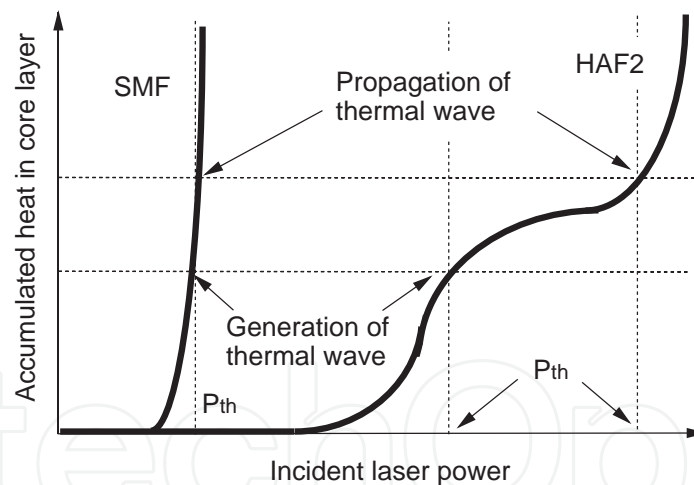


Figure 23. Schematic view of incident laser power vs accumulated heat in hot zone for HAF2 and SMF.

When the light power is small, the heat generated in the hot zone flows into the adjacent cladding layer, and the rise in the temperature of the zone is prevented. However, if light with a threshold power P_{th} and above enters the hot zone, it becomes difficult for all the generated heat to escape into the cladding layer, and part of the heat accumulates in the hot zone.

In the SMF, the accumulated heat raises the temperature in the hot zone and a thermal wave, *i.e.*, fiber fuse, is generated at the center of the zone. The thermal wave then rapidly increases in size and starts to propagate toward the light source as shown in Figure 23.

On the other hand, in HAF2, a large P_0 value is required to obtain sufficient accumulated heat for both the generation and propagation of a thermal wave, compared with that in the SMF.

Several researchers observed the dynamics of fiber fuse termination near a splice point between a HAF and an SMF by using a high-speed camera [42], [46], [48], [51].

Takenaga *et al.* reported that when a laser light of $P_0 = 8.1$ W and $\lambda_0 = 1.55$ μm was input into HAF2+, a fiber fuse was generated at the splice point between the HAF and the SMF, propagated about 100 μm in the direction of the light source, and then stopped [42]. Kurokawa and Hanzawa [46] defined the length between the splice point and the termination point of fiber fuse as a penetration length L_p . In this case, $L_p \simeq 100$ μm .

Similarly, Kurokawa and Hanzawa investigated the power dependence of both the propagation velocity v_f for the SMF and L_p for HAF2 at $\lambda_0 = 1.48$ μm [46]. When a laser light of $P_0 = 8.1$ W was input into HAF2, the observed v_f for the SMF was 1.1 m/s and L_p for HAF2 was $\simeq 80$ μm .

As shown in Figure 19, even if a high power of 9 W was input into HAF2, a fiber fuse with a high peak temperature of about 80,000 K was generated at the center of the heated core, but it did not propagate forward the light source. This phenomenon, in which the propagation of a fiber fuse is controlled, is in good agreement with the experimental results observed by Takenaga *et al.* and Kurokawa and Hanzawa [46] for HAF2.

On the other hand, Kurokawa and Hanzawa reported that $v_f = 1.3$ m/s and $L_p = 110$ μm when a laser light of $P_0 = 12.0$ W (6.0 W at both 1.48 μm and 1.55 μm) was input into HAF2 [46]. This behavior for HAF2 cannot be explained by our calculation described above. As shown in Figure 22, a fiber fuse, generated at the splice point between the HAF2 and the SMF, was expected to maintain propagation in the direction of the light source when $I_{th} = 12.2$ MW/cm² ($P_0 = 12.0$ W). However, it was reported that the fiber fuse propagated only about 120 μm , and then stopped.

Furthermore, they reported that the hole part in the HAF disappeared in the domain in which the fiber fuse penetrated [46]. They considered that the plasma density of the core decreased in connection with the disappearance of the hole part and that the propagation of a fiber fuse can be controlled even if a high power of 10 W order is input into an HAF. In practice, they observed the dynamics of fiber fuse termination near the splice point between HAF2 and the SMF and found that the termination was accompanied by the evolution of a gas jet in the case of $P_0 = 12$ W [48] and 18.1 W (6.6 W at 1.48 μm and 11.5 W at 1.55 μm) [51].

In order for the hole part to disappear with the gas jet, it is necessary for the (first) cladding layer inscribed in this hole part to be destroyed by the incident high power.

We considered the destruction of the cladding layer using our heat conduction model, the results of which are described below.

7. Destruction mechanism of inner cladding layer of HAF

The internal core space of an HAF heated to an elevated temperature is shielded from the external conditions. Thus, with increasing temperature, the internal pressure increases and

the internal volume decreases. Dianov *et al.* reported an internal core temperature of about 10,000 K and an internal pressure of about 10,000 atmospheres (1 GPa) at the time of fiber fuse evolution [72].

In HAF2, $D_{hole}/2 = 9.0 \mu\text{m}$ and $r_c = 4.5 \mu\text{m}$. Therefore, the thickness h of the first cladding layer was $4.5 \mu\text{m}$ before the core was heated to a high temperature. When the core is heated to a high temperature and the internal pressure p reaches 1 GPa, the first cladding layer is partially melted by heat transmitted from the core and h becomes smaller than its initial value ($4.5 \mu\text{m}$).

We consider a tensile stress σ_θ acting on the inner wall of the first cladding layer with thickness h , as shown in Figure 24.

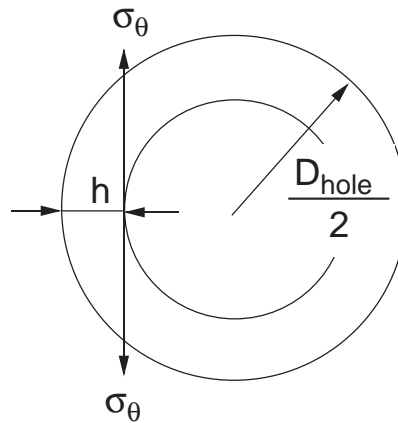


Figure 24. Tensile stress acting on inner wall of first cladding layer in HAF.

σ_θ is related to p by the following expression [96]:

$$\sigma_\theta = \frac{D_{hole}^2 - 2D_{hole}h + 2h^2}{2D_{hole}h - 2h^2} \cdot p. \quad (30)$$

σ_θ increases with increasing p . If σ_θ exceeds the ideal fracture strength σ_0 of the silica glass, a crack will generate on the inner wall of the first cladding layer.

On the other hand, it is well known for various solid materials that the σ_0 value is related to the Young's modulus E of the material by the following equation [97]:

$$\sigma_0 \approx E/10. \quad (31)$$

By using Eq. (31) and $E = 73 \text{ GPa}$ for silica glass, we can estimate σ_0 to be approximately 7.3 GPa.

For the HAF2, we estimated the relationship between h and the tensile stress σ_θ acting on the inner wall of the first cladding layer for $p = 1 \text{ GPa}$ using Eq. (30). The calculation result is shown in Figure 25.

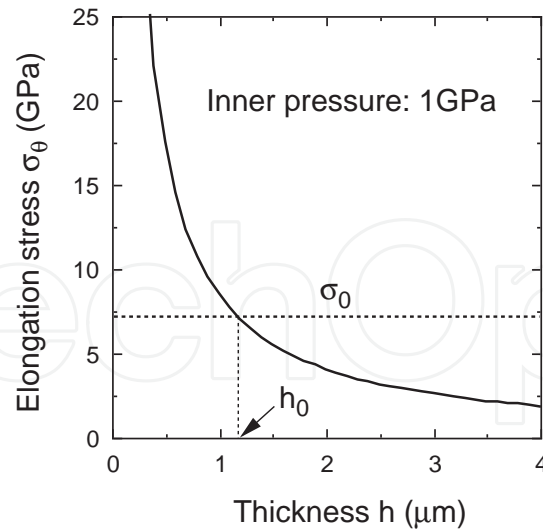


Figure 25. Thickness vs tensile stress acting on inner wall of cladding layer in HAF2.

σ_θ increases with decreasing h . It was found that when h decreases to a critical thickness h_0 ($\sim 1.2 \mu\text{m}$), σ_θ becomes to σ_0 ($\sim 7.3 \text{ GPa}$). That is, σ_θ becomes larger than σ_0 when $h < h_0$. This means that the inner wall of the first cladding layer will crack and be destroyed when $h < h_0$.

Silica glass has a melting temperature of $T_m = 1,973 \text{ K}$. If solid silica glass is heated above T_m , it will become a liquid "melt" and its mechanical properties, such as tensile tolerance, will be lost.

If the heat conduction model discussed above is used, the temperature distribution along the internal radial direction can be estimated for the HAF2.

We can estimate the radial distance (equivalent to h in Figure 24) from the outer wall of the first cladding layer with temperature T_a to an inner point at which T reaches T_m using the heat conduction model. Then, the minimum power of incident laser light necessary for $h < h_0$ to be satisfied can be determined by estimating the h value when laser light with various powers enters the HAF2.

For incident laser powers P_0 of 4–10 W with $\lambda_0 = 1.55 \mu\text{m}$, the temperature distribution in the first cladding layer as a function of the radial distance h' was calculated for the HAF2. The result is shown in Figure 26.

The horizontal axis h' in Figure 26 represents the distance between the outer wall of the first cladding layer and an inner point located closer to the core center.

When P_0 is 4 W or less, the temperature T in the cladding layer is lower than T_m , and the cladding layer is not destroyed.

On the other hand, when P_0 is 5 W and above, T increases with increasing h' . When $P_0 = 10 \text{ W}$, T reaches $\sim T_m$ at $h' \sim 1.2 \mu\text{m}$. This value of h' ($\sim 1.2 \mu\text{m}$) is the same as the threshold value of h_0 ($\sim 1.2 \mu\text{m}$) for crack generation on the inner wall of the cladding layer. Therefore, the destruction of the cladding layer is predicted when laser light with $P_0 \geq 10 \text{ W}$ enters the HAF2.

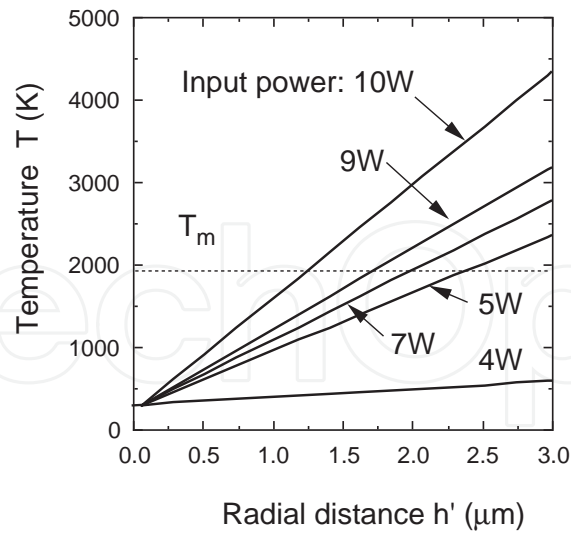


Figure 26. Temperature field in first cladding layer of HAF2 when $P_0 = 4\text{--}10\text{ W}$ at $\lambda_0 = 1.55\text{ }\mu\text{m}$.

If a thermal wave propagates along the fiber axis, because of the pressure difference of about 10,000 atmospheres between the internal core and the air hole layer, the destruction of the cladding layer will change the propagation direction of the thermal wave from the axial direction to the radial direction. As a result, the thermal wave will propagate toward the air hole layer with a low pressure (about 1 atmosphere). This is the reason for the observation of a gas jet reported by Kurokawa *et al.* [48].

When the thermal wave propagates into the air hole layer, the hole layer disappears as a result of thermal heating and the core temperature decreases owing to the departure of the thermal wave. Such cooling of the core will prevent the generation of a new thermal wave in the core, and the propagation of the thermal wave will stop at this time.

Kurokawa and Hanzawa [46] reported that when laser light with a high power entered HAF2, the increase in penetration length started at an incident power of 8 W.

As described above, if the incident power increases from 9 W to 10 W, the cladding layer is destroyed and the direction of propagation of the thermal wave changes to the radial direction, and the air hole layer vanishes owing to the melting of the cladding layer.

There is a slight time delay τ for a crack propagating from the inner surface to the outer surface of the first cladding layer. The crack generated on the inner surface of the first cladding layer grows and propagates to the outer surface of the cladding layer. When the crack reaches the outer surface, the first cladding layer is destroyed because of the pressure difference of about 10,000 atmospheres between the internal core and the air hole layer.

The crack propagation rate V_c of the silica glass is related to the sonic rate V_s of the glass as follows [98]:

$$0 \leq V_c \leq 0.38V_s. \quad (32)$$

The value of V_s for silica glass is 5,570 m/s. For a crack propagating through a small length of $\sim 1.2\text{ }\mu\text{m}$ ($= h_0$), the minimum time delay τ_m was estimated to be

$$\tau_m \equiv \frac{h_0}{0.38V_s} = 5.7 \times 10^{-10} \text{ s}. \quad (33)$$

This time delay is not dependent on the incident power, as indicated by Eq. (32), and the propagation velocity v_f of the thermal wave increases with increasing incident power.

We assumed that τ for the HAF2 corresponded to the time (50–90 μs) for rapid rise in the core temperature after the incidence of fiber fuse, which propagated in the SMF. If we assume that $\tau \sim 80 \mu\text{s}$ and the penetration length L_p is the product of v_f and τ , the L_p values at a incident light of $P_0 = 8.1 \text{ W}$ and 12.0 W are $88 \mu\text{m}$ and $104 \mu\text{m}$. These values are fairly good agreement with the experimental results ($\sim 80 \mu\text{m}$ and $110 \mu\text{m}$) reported by Kurokawa and Hanzawa [46].

In closing, we should comment on the fiber fuse propagation with a long-period damage track, which was observed in the HAF2 with d_h of smaller than r_c [46], [48]–[50]. The most striking characteristic of this phenomenon is the long period (several 100 μm order) of the cavities, which were generated by entering of a relatively low power (about 1.5–4.5 W) into HAF2.

The long period damage tracks such as those in HAF2 were reported by Bufetov *et al.* [99]. They found that such a phenomenon was observed as a result of the interference of LP_{01} and LP_{02} modes excited in an optical fiber with a W-index profile. However HAF2 is a step-index optical fiber, and only LP_{01} (or TE_{11}) mode can be excited in HAF2 at 1.48 and/or 1.55 μm . Therefore, it is very difficult to consider that the mode interference is responsible for the long period damage tracks observed in HAF2.

Instead of the mode interference, we consider that this phenomenon may relate to a thermal lense effect [63], [101]. The focal length F of thermal lense effect is given by (see Appendix)

$$F = \frac{n_0 \pi \kappa \omega_0^2}{\alpha P l (\partial n / \partial T)}, \quad (34)$$

where n_0 ($= 1.46$) is the characteristic refractive index of the core layer, P is the incident power of the light reflecting from the cavity wall, which is estimated by Eq. (24). ω_0 ($\sim 4.5 \mu\text{m}$) is the spot size radius of the laser beam when optical power in the optical fiber was assumed to take on Gaussian distribution, $\partial n / \partial T$ ($= 1.23 \times 10^{-5} \text{ K}^{-1}$ [5]) is the thermal coefficient of refractive index for silica glass, and l is the length of the heating core, where α exhibits large value.

As F is inversely as the product of α and P , large F value may be obtained by small α and/or P value, which is comparable with observed long period of the cavities. If we assume $\lambda = 9.2 \text{ W/mK}$ [5], $l = 20 \mu\text{m}$, and $\alpha = 5 \times 10^4 \text{ m}^{-1}$, the F value at $P = 0.158 \text{ W}$ ($P_0 = 4.5 \text{ W}$) can be estimated to about $440 \mu\text{m}$ by using Eq. (34). This value is fairly good agreement with the observed period ($460 \mu\text{m}$) of the cavities [46], [48]–[50].

The cause of mechanism of the long-period damage track has yet to be sufficiently clarified. It largely depends upon future multilateral studies.

8. Conclusions

We investigated the unsteady thermal conduction status in a single-mode optical fiber by numerical computation in order to visualize the mode of fiber fuse propagation. We assumed that the vitreous silica optical fiber underwent pyrolysis at elevated temperatures to form SiO_x ($x \sim 1$). We also proposed a model in which the optical absorption coefficient of the core layer increased with increasing molar concentration of SiO_x . By using the model, we calculated the temperature distribution in the fiber with the explicit finite-difference method. It was found that when a short core with $40 \mu\text{m}$ length was heated to $2,923 \text{ K}$ and a 2 W laser light (wavelength of $1.064 \mu\text{m}$) entered the core layer of an SMF-28 optical fiber, a thermal wave, *i.e.*, a fiber fuse, with a peak temperature of about $34,000 \text{ K}$ was generated at the boundary of the heating region near the light source. The fiber fuse was enlarged and propagated toward the light source at a rate of about 0.54 m/s . The calculated propagation velocity of the fiber fuse was in agreement with the experimental value. Moreover, the average temperature of the radiated region of the core layer was less than $7,000 \text{ K}$ at a time of 4 ms after the generation of the fiber fuse and gradually approached a temperature of about $5,700 \text{ K}$. The final average temperature was close to the experimentally reported values.

We evaluated the threshold power of fiber fuse propagation in hole-assisted fibers (HAFs) using the finite-difference method and the model proposed by Takara *et al.* The HAFs with ratios of hole-space distance to core diameter of 3 and 4 exhibited fiber fuse propagation when a $1.55 \mu\text{m}$ laser with a power of 4 W was input into the core layer, as observed for an SM optical fiber.

On the other hand, the HAF with a ratio of hole-space distance to core diameter of 2 exhibited no fiber fuse generation or propagation when a $1.55 \mu\text{m}$ laser with a power of 10 W was input into the core layer.

Furthermore, when the incident power was 5 W and above, the temperature of the central core increased owing to the absorption of a large amount of power, causing the melting of the first cladding layer adjacent to the heated core. Thus, the thickness of the first cladding layer decreased below the value at which the solid cladding layer could be maintained, and the cladding layer was destroyed following the disappearance of the air hole layer. The destruction of the cladding layer caused the direction of the thermal wave to change from the axial direction to the radial direction, stopping the propagation of the thermal wave. By using this phenomenon, Kurokawa and Hanzawa proposed a novel fiber fuse terminator composed of a short length of HAF [100].

Appendix: Focal length of thermal lens effect

If part of the core layer is heated by light absorption, the refractive-index gradient in the core is induced by the thermal coefficient of the refractive index $\partial n / \partial T$ of the silica glass and the temperature distribution ΔT in the core layer. The refractive index n of the heated core is expressed as follows:

$$n(r, t) = n_0 + \frac{\partial n}{\partial T} \Delta T(r, t) \quad (35)$$

where n_0 ($= 1.46$) is the characteristic n value of the core layer, r is the radial distance from the center of the optical fiber, and t is time, respectively.

If we assume that optical power in the optical fiber takes on Gaussian distribution, ΔT in the core layer is given by [63], [101]

$$\Delta T(r, t) = \frac{\alpha P}{4\pi\lambda} \left[\ln \left(1 + \frac{8Dt}{\omega_0^2} \right) - \frac{16Dt}{\omega_0^2 + 8Dt} \frac{r^2}{\omega_0^2} \right] \quad (36)$$

where α is the absorption coefficient, P is the incident optical power, ω_0 is the spot size radius of the laser beam, and λ is the thermal conductivity of the silica glass, respectively. Parameter $D = \lambda / C_p \rho$, where C_p and ρ are the specific heat and density of the silica glass.

Substitution of Eq. (36) into Eq. (35) gives

$$n \cong n_0 \left[1 + \delta \left(\frac{r}{\omega_0} \right)^2 \right], \quad (37)$$

$$\delta = -\frac{2\alpha P}{4n_0\pi\lambda} \left(\frac{\partial n}{\partial T} \right) \frac{8Dt}{\omega_0^2 + 8Dt}. \quad (38)$$

When refractive index of the core layer takes a radial distribution as shown in Eq. (37), propagating laser beam will be focussed as a result of the thermal lens effect. In this case, the focal length F is given by [63], [101]

$$F(t) = \frac{n_0\pi\lambda\omega_0^2(\omega_0^2 + 8Dt)}{\alpha Pl(\partial n/\partial T)(8Dt)} = F_\infty \left[1 + \frac{t_c}{2t} \right], \quad (39)$$

$$F_\infty = \frac{n_0\pi\lambda\omega_0^2}{\alpha Pl(\partial n/\partial T)}, \quad (40)$$

$$t_c = \frac{\omega_0^2}{4D} \quad (41)$$

where l is the length of the heating core, where α exhibits large value. In typical SM fiber, $\lambda = 9.2$ W/mK, $C_p = 788$ J/kgK, $\rho = 2,200$ kg/m³ [5], and $\omega_0 \sim 4.5$ μ m. If we insert these values into Eqs. (39)–(41), we obtain $t_c \sim 0.95$ μ s. This means that $F \cong F_\infty$ when t is 10 μ s or above. If we assume $P = 2$ W, $l \sim 40$ μ m, $\alpha = 5.6 \times 10^4$ m⁻¹ [5], and $\partial n/\partial T = 1.23 \times 10^{-5}$ K⁻¹ [5], F is given by

$$F \cong F_\infty \sim 15.5 \mu\text{m}$$

This F value is of the same order of the observed interval and/or large front size of the cavities [11], [23].

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