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Basics on Radar Cross Section Reduction Measurements of Simple and Complex Targets Using Microwave Absorbers

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1. Introduction

The research of Radar Cross Section (RCS) of simple and complex objects is decisively important to identify targets such as aircraft, missiles, rockets, ships and other objects, with the purpose of improving or rendering difficult their radar visibility in various frequency ranges. The use of RCS measurements of targets have expanded to more than solely military applications in the identification and control processes of defense systems (Burgess, 1988).

Higher the RCS value is, easier it becomes to detect and identify an object. However, when these targets present different geometrical forms and different types of electromagnetic radiation absorber materials (ERAM) on their surfaces, they can become stealthy and practically invisible to radars at determined frequency ranges.

In order to make target identification more precise, it is indispensable to analyze and understand the RCS patterns generated by the targets. These patterns represent the reflection mechanisms in the interaction process of the wave with the target, i.e., the interaction of the wave with the aspects of the target's geometry and the material's physical-chemical characteristics of its surface (Dybdal, 1987).

RCS measurements aim to determine the equivalent effective area of the target when it is impinged by a radar wave. In other words, it is the ratio between the electromagnetic energy irradiated by radar over a target and the energy scattered by it. The scattering measurements can be performed in monostatic condition, whereby the electromagnetic waves reflected by the target are measured in the same direction as the emitting source (radar), or in bistatic condition, when the reflected waves are detected in other directions. The present work describes experimental studies of RCS measurements of targets with simple and complex shapes and the RCS reduction by using ERAM in the microwave frequency range of 5 – 12 GHz (C and X bands). This chapter intends also to give some highlights about the theory involved and some measurement topics concerning target reflectivity, calibration techniques, enhancement methods and some experimental results achieved in this research performed at Materials Division of the Institute of Aeronautics and Space from Brazil.

2. Main definitions

When an electromagnetic wave focuses on an object the energy is spread in all directions. The spatial distribution of energy depends on the target geometry, material composition, the operating frequency and polarization of the incident wave. This distribution of energy is called scattering and the material is often called target (Blake, 1986).

Based on this principle, we can define the radar cross section, or RCS, as a measure of the power that returns to source or reflects in a given direction, normalized in relation to an incident wave power density. The purpose of normalization is to remove the effect of distance and facilitate the description of the cross section independent of the distance between the target and radar (R). The RCS is defined as shown in equation 1 (Bhattacharyya & Sengupta, 1991).

$$\sigma = 4\pi \lim_{R \rightarrow \infty} R^2 \frac{|\vec{E}^S|^2}{|\vec{E}^I|^2} = 4\pi \lim_{R \rightarrow \infty} R^2 \frac{|\vec{H}^S|^2}{|\vec{H}^I|^2} \quad (1)$$

where:

σ : radar cross section of the target (m^2);

\vec{E}^S : reflected or scattered electric field (V/m);

\vec{H}^S : reflected or scattered magnetic field (A/m);

\vec{E}^I : incident electric field (V/m);

\vec{H}^I : incident magnetic field (A/m).

The scattered electric and magnetic fields are due to the presence of a target, so, the total field is the sum of the incident and the scattered fields (equation 2):

$$\vec{E}^T = \vec{E}^I + \vec{E}^S \quad (2)$$

The RCS unit is usually given in square meters, or expressed in dB, relative to one square meter (dBm^2 or dBsm) as in equation 3 (Currie, 1989).

$$\sigma(\text{dBm}^2) = 10 \log_{10}[\sigma(\text{m}^2)] \quad (3)$$

These concepts can be applied in the radar equation (Skolnik, 1990), correlating the received power in terms of transmitted power, scattering, distance and antennas gain (equation 4).

$$P_R = \left(\frac{P_T G^2 \sigma \lambda^2}{(4\pi)^3 R^4} \right) \quad (4)$$

where:

P_R : radar received power (W);

P_T : radar transmitted power (W);

R : distance between radar and target (m);

σ : radar cross section of the target (m^2);

G : radar antenna gain (dimensionless);

λ : wavelength (m).

The received power by the antenna from the transmitted radar pulse is directly related with the physical characteristics of the target through the backscattering coefficient. The value of this backscattering coefficient is basically dependent on the following factors (Jenn, 1995):

- the target geometry and surface roughness;
- the target material composition (electrical and/or magnetic properties);
- the wavelength and polarization of the radar; and
- the aspect angle related with the incident wave.

The conceptual definition of RCS includes the fact only one part of the radiated energy reaches the target. The RCS of a target (σ) can be most easily visualized as the product of three factors:

$$\sigma = \text{Projected cross section} \times \text{reflectivity} \times \text{directivity}$$

The reflectivity is defined as the intercepted radiated (scattered) power by the target. The directivity is given by the ratio of the backscattered power into the radar's direction to the power that would have been backscattered, considering an uniform scattering in all directions (isotropic).

2.1 Scattering matrix

In order to determine the dependence of the RCS in relation to the polarization of the wave, we must consider the relationship between the transmitted (t) and the received (r) fields, in terms of the horizontal and vertical components of linear polarization of the wave, E_H and E_V , respectively, where the index H denotes horizontal polarization and V the vertical polarization. Then, E_H and E_V can be expressed in terms of the reflectivity of a target illuminated by both polarizations through the proportionality constant a_{ij} , where i denotes the polarization of the transmitter and j the polarization of the receiver (equation 5) (Crispin, 1968) or in matrix notation (equation 6):

$$\begin{aligned} E_H^r &= a_{HH}E_H^t + a_{VH}E_V^t \\ E_V^r &= a_{HV}E_H^t + a_{VV}E_V^t \end{aligned} \tag{5}$$

$$\begin{bmatrix} E_H^r \\ E_V^r \end{bmatrix} = \begin{bmatrix} a_{HH} & a_{VH} \\ a_{HV} & a_{VV} \end{bmatrix} \begin{bmatrix} E_H^t \\ E_V^t \end{bmatrix} \tag{6}$$

The constants a_{ij} shall be considered independent of the distance, but in complex notation due to its phase relationship between the electric field components. For a monostatic radar configuration, a_{HV} and a_{VH} are equal. Therefore, the scattering matrix defines the relationship between amplitude and phase components of the electric fields transmitted and received.

A similar matrix to that one mentioned for linear polarization of the wave can be obtained for elliptical and circular polarizations, using the constants of proportionality describing the left or right hand polarization (Crispin, 1968).

2.2 Frequency regions

When a target has very small physical dimensions compared to the wavelength of the incident wave, it is considered that your analysis is being done in the so called *Rayleigh* region (Blake, 1986). In this region, the shape of the object does not influence in determining their RCS, and for some types of objects the RCS is determined from the volume, instead of considering the dimensions and physical forms. For targets that are comparable in size to

the wavelength of incident wave, the RCS varies depending on the frequency and is called the resonant region or *Mie* region.

When the dimensions of the target are large compared with the wavelength of incident wave, the RCS can be determined using the methodology of geometrical optics or by the method of optical physics, and this region is called the optical region. In the following sections, the analysis of some RCS targets of simple and complex geometry is shown in the optical region. Figure 1 is a RCS curve of a sphere as a function of the ratio of the target radius (a)/ wavelength (λ), normalized in the optical region. The analysis of this figure shows that there are the distinct regions discussed above. Although it is a perfectly conducting sphere, this behavior is observed for all types of targets (Currie, 1989; Bhattacharyya & Sengupta, 1991).

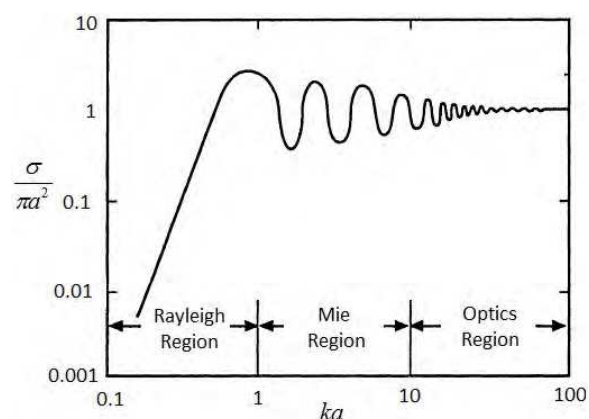


Fig. 1. Normalized RCS of a sphere as a function of ka (where $k=2\pi/\lambda$).

3. Radar cross section reduction measurements

RCS measurements are performed for many reasons; the main one is to verify target detection limits by a radar system to which it is subjected, verifying conformity of the practical models, designed by theoretical equations (Kouyoumjian, 1965).

The measurement as a whole is a complex task due to the many factors that may affect these measurements. Instrumental errors, spurious interferences and reflections are some of contributions to degrade the quality of the data. These problems are compounded when one is interested in reducing the RCS of an object, as in this case, the magnitude of these effects can overshadow the true RCS values.

Many methods have been proposed and used for the measurement of several types of targets. Depending on the size of the targets and radar frequencies used, RCS measurements can be performed on outdoor or indoor ranges, in the last condition, inside anechoic chambers. In measurements, it is important that the radar is illuminated by an electromagnetic wave which is uniform in phase and amplitude. For practical purposes, the maximum tolerance for amplitude variation over a target is 0.5 dB, and the phase should not deviate more than 22.5°. These conditions denote the far-field condition (Balanis, 1982; Jasik & Johnson, 1984), given by:

$$R \geq \frac{2d^2}{\lambda} \quad (7)$$

where:

R is the distance between radar and target;

d is the largest dimension of the target; and

λ is the wavelength of the radar.

This condition ensures good measurements. Errors produced by the instrumentation should neither exceed 0.5 dB nor vary in time in order to avoid instability in the measurement of the RCS patterns. Thus, it is decisive the careful selection of the experimental parameters. In this case, the dynamic range of the system should be at least 40 dB when measuring targets with small RCS. Dynamic range values in the order of 60 dB or higher are preferable when RCS reduction studies are conducted or when absorber materials are used. Another important factor to be taken into account is the target support structure that should not interfere with the incident wave, however in practice such condition isn't always possible.

Analysis of the electromagnetic energy scattering by metallic objects is very important in the understanding of RCS of targets, in the same way that reflections of dielectric and magnetic surfaces are important when studying RCS reduction. Within this context, RCS analysis of targets with simple shapes is fundamental to support the understanding of RCS patterns of targets with complex shapes.

To evaluate the electromagnetic behavior of targets, many methods have been proposed and experimentally used for many decades with well accepted results (Birtcher & Balanis, 1994) and the RCS measurement errors depend on the nature of the target under test, the distance at which this target is being measured and the place of measurements.

Systems are projected in such way that respect the parameters described above. However, they present technical challenges, making adequate the use of experimental procedures that involve new techniques that can minimize errors. When an anechoic chamber is used, the emissions and reflections of spurious radiation are controlled and minimized by using commercial off the shelf ERAM inside the chamber, becoming the background noise levels of this radiation almost null. On the other hand, by using the outdoor range, the measurements are affected by environment variations, therefore needing greater control of the parameters.

Even in measurements performed in indoor range, the RCS patterns of the targets may become impaired due to the occurrence of noise in the system or on account of low backward radiation contribution of the targets with lower RCS.

3.1 Basic instrumentation

The basic instrumentation required for RCS measurements consists of four subsystems that can be controlled by a central station; these subsystems are: positioners and drivers, receiver, transmitter and data acquisition system.

Using a simple setup and placing the transmitter (TX) and receiver (RX) antennas in the scheme showed in Figure 2, it is possible to measure the RCS of targets in different frequency ranges. The distance between both antennas needs to be tested to eliminate the radiation coupling between them.

In order to have good precision, the transmitter must have means to provide enough power to allow a good signal/noise ratio for the measurement system and it is necessary to take

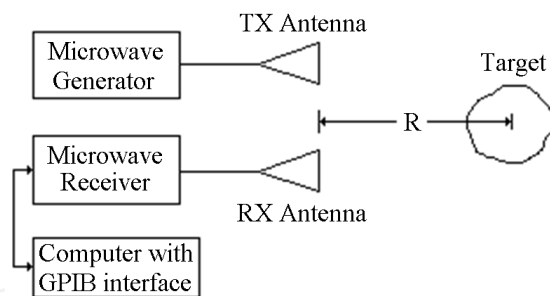


Fig. 2. RCS measurement setup (R is the distance between the antennas and the target).

care with the alignment between the transmission/reception antennas and the target. The use of a laser beam helps in the alignment of the system improving the precision of the measurements. The support column for the target, called as pylon, needs to be recovered with ERAM in order to avoid any possible contribution of reflected waves that prejudices the target characterization.

Figure 3 shows a system used in this study that basically consists of two antennas, one transmitter and one receiver mounted on a tower keeping a certain distance from each other. The target is mounted on a dielectric support and this one is mounted on a positioner which will allow recording the RCS patterns. The transmission is made through a microwave generator that feeds, by a low loss coaxial cable, the antenna input terminals. A spectrum analyzer can be used as a receiver that collects the signals from the receiving antenna. The system has a positioner controller (driver) that controls the rotational speed, azimuth angle and limits. Some equipment is in a control room, where the user monitors the tests through a computer with a GPIB interface.

Figure 3 shows the system composed by:

- Target under test (square flat plate with 0.2 m side);
- Pyramidal microwave absorbers;
- Horn antennas to the 8.2 – 12.4 GHz frequency range;
- Low loss coaxial cables; and
- Microwave generator.

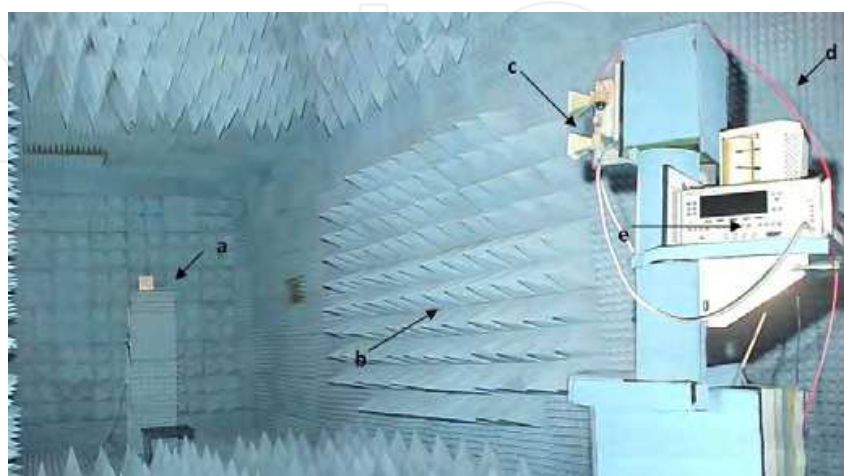


Fig. 3. Anechoic chamber view assembled with the RCS measurement system (courtesy of IFI/DCTA, Brazil).

Figure 4 shows the internal view of the control room (shelter), which is integrated with the instrumentation located inside the anechoic chamber. This figure shows: (a) antenna positioner controllers; (b) spectrum analyzer (receiver) and (c) computer.



Fig. 4. Internal view of the control room (courtesy of IFI/DCTA, Brazil).

3.2 Amplitude calibration methods

There are two main methods for calibration of systems for RCS measurements: direct and indirect calibrations. The direct calibration involves the use of reference targets with well known values of RCS, such as spheres, flat plates, dihedrals and dielectric lens. The RCS of these targets can be accurately inferred by its physical sizes, to provide a radar return signal that can be compared to the signal of a target under test with unknown value of RCS. In some cases, the reference target may be in a different position relative to the target under test and a modified form of the radar equation is used to estimate the difference, as seen in equation 8:

$$\sigma_u = \left[P_r \left(\frac{R_u}{R_r} \right)^4 \left(\frac{F_r}{F_u} \right)^4 \right] \sigma_r \quad (8)$$

where:

σ_u : RCS of the target under test (m^2);

P_r : received power ratio between the reference target and target under test (dimensionless);

R_u : distance between target under test and radar (m);

R_r : distance between reference target and radar (m);

F_u : propagation factor of the target under test (dimensionless);

F_r : propagation factor of the reference target (dimensionless); and

σ_r : RCS of the reference target (m^2).

From equation 8, the propagation factors F_r and F_u contain information about the conditions of propagation between the radar and the two targets, including any atmospheric attenuation, scattering or even any undesired multiple reflection, as ground reflection that may be present. If the two factors are the same during measurements, equation 8 is reduced to equation 9:

$$\sigma_u = P_r \left(\frac{R_u}{R_r} \right)^4 \sigma_r \quad (9)$$

The accuracy of this calibration method depends on the accuracy of the RCS reference target and the assumption that there are no other targets or significant sources of reflection on the measuring environment and the propagation factor is well known.

The second method of amplitude calibration is known as the indirect calibration method or closure. This method involves precise measurements of the characteristics of the radar system or the transmission and reception system by measuring the received power of a target under test with unknown RCS, and the calculation of RCS is done by using the radar range equation (equation 10) below:

$$\sigma_u = \frac{P_R (4\pi)^3 (R_u)^4 L_T L_R}{P_T G^2 \lambda^2 (F_u)^4} \quad (10)$$

where:

- σ_u : RCS of the unknown target (m²);
- P_R : received power from the unknown target (W);
- L_T : transmitter losses (dimensionless);
- L_R : receiver losses (dimensionless);
- R_u : distance between radar to unknown target (m);
- P_T : transmitted power (W);
- G : radar antenna's gain (dimensionless);
- λ : wavelength (m), and
- F_u : propagation factor (dimensionless).

For this method is considered accurate, the parameters of the radar should be carefully measured, the received power must be precisely determined and the propagation factor should be equal to unity. The errors associated with this technique can occur in the measurements of radar parameters such as received power and also in conditions where the propagation factor is not equal to unity. One advantage of the indirect technique is that the reference target is not required.

3.3 Enhancement measurement techniques (active cancellation)

In order to reduce some error sources present in RCS measurements such as coupling between antennas, reflections in the anechoic chamber, reflection of target support and poor dynamic range, it can be used an active noise cancellation circuit which employs a phase cancelling technique.

A result of works performed at Materials Division/IAE/DCTA in Brazil shows an experimental set-up developed to reduce the error sources presented in indoor RCS measurements in C-band (5.8 to 6.4 GHz). By means of this research it was possible to perform comparisons, with and without the developed system, and observe its influence in measurements of simple objects.

By proposing the implementation of the system, it is expected to allow detection of small RCS targets by increasing sensitivity and dynamic range, so the effective study of RCS reduction can be established. The complete measurement system has a simplified block diagram shown in Figure 5.

The operation principle of the device is based on the detection of spurious signals and the application of the principle of phase cancelling, by generating a signal of equal amplitude

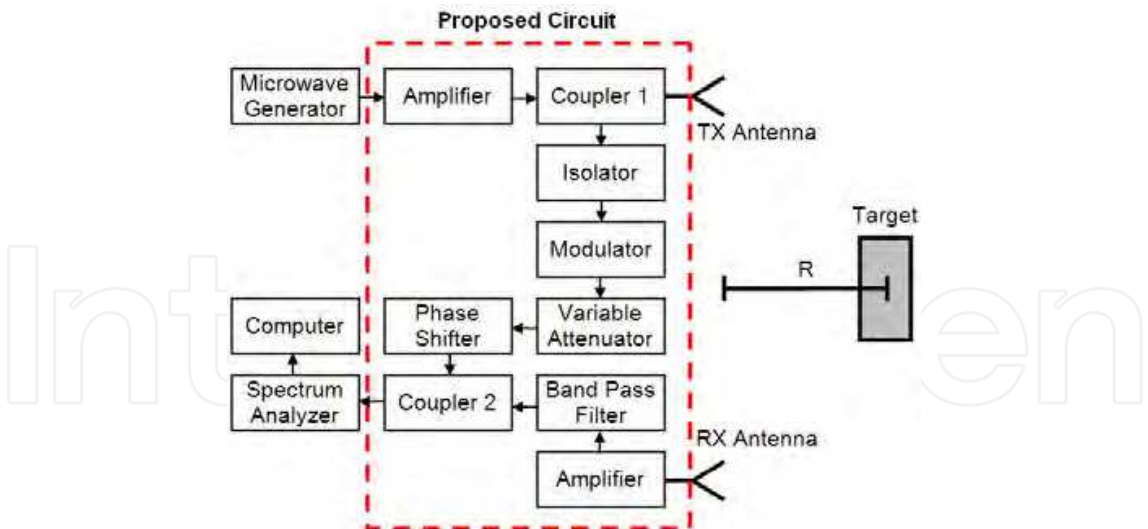


Fig. 5. Block diagram of the measurement system with the active noise cancellation circuit.

and opposite phase. Thus, after operation of the system only the signal of the target under test is expected to be detected. In this case, errors inherent to the RCS measurement systems in an indoor or outdoor range are reduced.

In accordance with Figure 5, operation of the developed device consists of a sample of the signal transmitted by the radar through the directional coupler 1. This signal goes through an isolator, followed by the modulator that performs phase and amplitude modulation (with fine tuning provided by the variable attenuator and phase shifter) and are combined in the directional coupler 2 with the interfering signals. Figure 6 shows the components used, such as: isolator, attenuator, coupler, filter and etc.

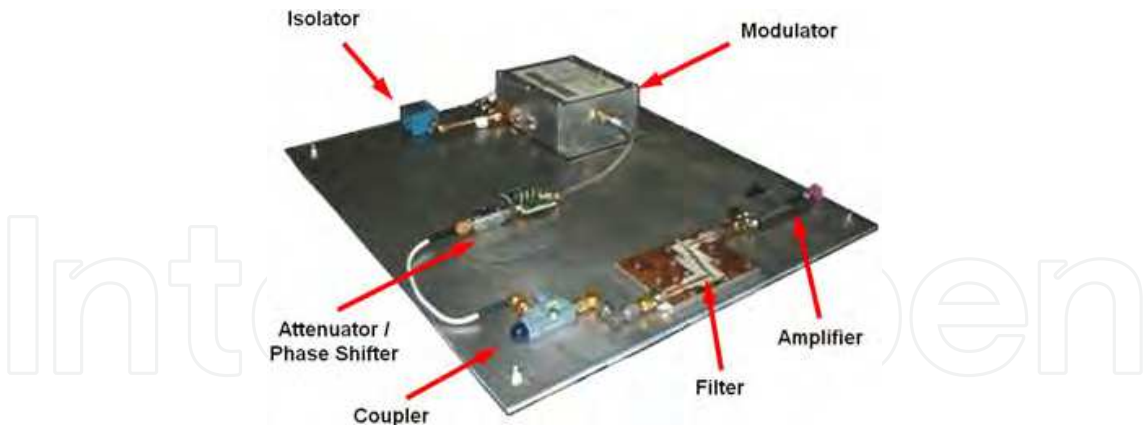


Fig. 6. View of the designed circuit assembled for C-band.

For the evaluation of the system, this circuit was tested by using an anechoic chamber with dimensions of 9.5 m x 4.5 m x 4.5 m available at IFI/DCTA. For this, two corrugated horn antennas were installed, with a transmitter and a receiver and a flat plate measuring 0.3 m x 0.3 m was used as a target under test, at frequencies of 5.9, 6.0, 6.2, and 6.4 GHz. Firstly, the noise level in the chamber was measured with and without the proposed circuit by rotating the azimuth positioner with no targets mounted on that. Some results are shown in Figure 7 and Table 1 presents the results obtained with the circuit for the frequency range.

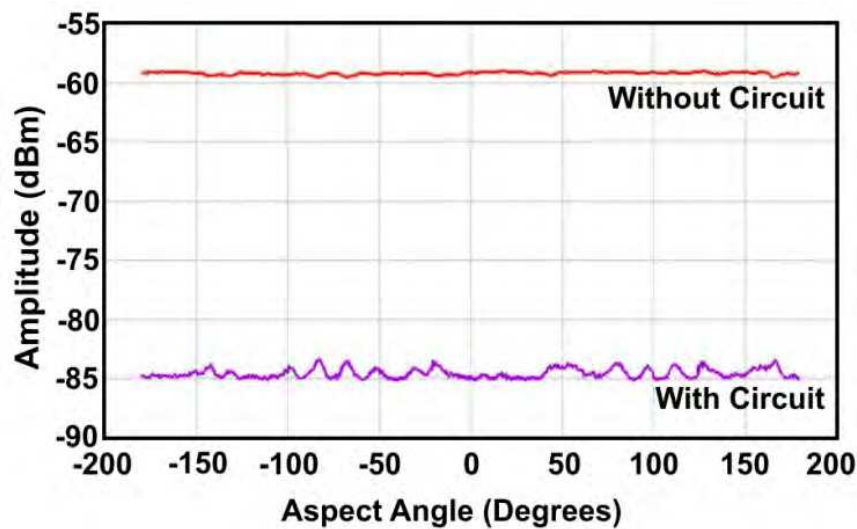


Fig. 7. Noise level of the anechoic chamber, with and without the circuit, at 5.9 GHz.

Frequency (GHz)	Noise level without the circuit (dBm)	Noise level with the circuit (dBm)	Reduction (dB)
5.9	-59	-85	26
6.0	-64	-84	20
6.2	-64	-85	21
6.4	-60	-82	22

Table 1. Anechoic chamber noise level reduction in C-band (deviation: 0.7 dB).

It is observed that due to the reflection from the anechoic chamber, added to the coupling between the antennas, the noise level is relatively high (approximately -59 dBm at 5.9 GHz).

Afterwards, a RCS pattern of the flat plate was measured without the circuit (Figure 8 - left) and it was observed a considerable deformation of the flat plate RCS pattern that can be assessed by foreseen results in literature (Ross, 1966) and experimental measurements (Miacci, 2002). After the circuit’s operation, where the interfering signals were reduced, a new RCS pattern of the flat plate was measured and it can be observed as being closer than expected, as seen in Figure 8 (right).

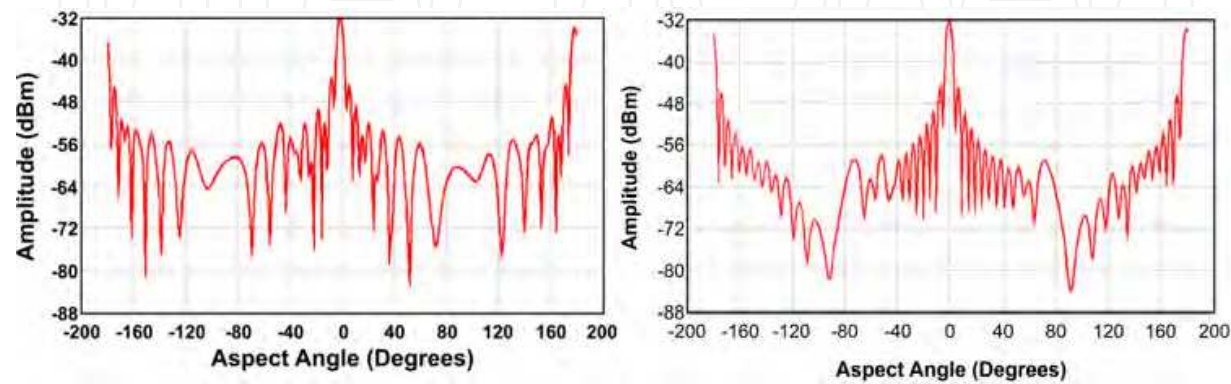


Fig. 8. RCS measurements of the flat plate (0.3 m x 0.3 m) without the circuit (left) and with the circuit (right) at 6.0 GHz.

This last RCS pattern evidences well defined null points and symmetry with a minimal contamination from external signals. It is also observed that the circuit does not influence the maximum peak, hence not interfering in the maximum RCS of the target under test.

Table 2 shows the minimum detectable RCS values and it is shown the increase of the probability of detection of smaller targets, associated to a higher dynamic range of the system, consequently, allowing the study of RCS reduction to be more effective when dealing with targets covered by high attenuation ERAM.

Frequency (GHz)	Detectable RCS without circuit (dBsm)	Detectable RCS with circuit (dBsm)
5.9	-09	-35
6.0	-16	-36
6.2	-15	-36
6.4	-11	-33

Table 2. Minimum detectable RCS values with and without the circuit (deviation: 0.7 dB).

The results denote that the RCS measurements performed with the developed and built circuit improved the RCS patterns with a remarkable reduction of interfering signals in the frequency range. This consideration takes into account the testing environment being almost completely free of spurious signals that reduce precision of measurement systems and can lead to false conclusions in analyses of RCS patterns. These preliminary measurements support other applications in bigger anechoic chambers or even in outdoor measurements.

4. Reflectivity characteristics of simple and complex shapes targets and RCS reduction by using ERAM

In this section it will be treated the reflectivity characteristics of simple and complex targets and discussed the experimental results of the RCS reduction research by using ERAM developed in Brazil.

4.1 Simple shapes targets

The electromagnetic theory allows the RCS calculation of targets that can be mathematically well defined, considering its size and physical forms. In practice this statement refers to objects with simple geometries. The solutions for simple objects are very important for two reasons, firstly, these objects can be considered as reference targets and they can be constructed and used as calibration references to measure complex geometry targets; second, approximations of equations used to determine the RCS of complex geometry objects can be made by detailed knowledge of the behavior of objects of simple geometries and their combinations (Miacci, 2002).

Table 3 shows the equations used for the RCS theoretical calculation for some simple geometry shapes in the optical region (Ruck, 1970; Knott et. al., 1993).

In the next sections is presented some experimental results achieved by the research group in RCS measurements of targets with simple and complex geometries and its RCS reduction when applying ERAM.

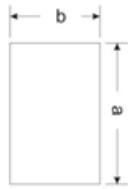
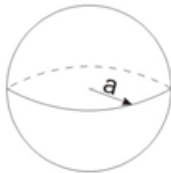

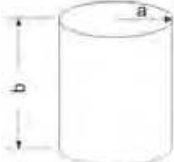
Geometry	RCS (m ²)
<div>Flat Plate</div> 	$\sigma = \frac{4\pi a^2 b^2}{\lambda^2}$
<div>Sphere</div> 	$\sigma = \pi a^2$
<div>Diedral</div> 	$\sigma = \frac{8\pi a^2 b^2}{\lambda^2}$
<div>Cylinder</div> 	$\sigma = \frac{4\pi a b^2}{\lambda}$

Table 3. RCS of some simple geometries in optical region.

4.1.1 Dielectric lenses (Luneberg reflectors)

In order to validate a RCS measurement setup, firstly, it can be used a certified reference target called Luneberg reflector. A Luneberg reflector (Figure 9 - left) is a sphere constituted of dielectric massive shells. Figure 9 (right) depicts a measured RCS pattern of this target using the setup described in section 3.1, in function of the aspect angles between 0 and 180° in the frequency of 9.375 GHz.

The maximum power observed in this pattern corresponds to the RCS value of 45 m², according to the certified value given by the Luneberg reflector’s manufacturer (Thomson CSF International Inc.). Using the relationship given by equation 9, it is possible to determine the RCS values of single targets in the same frequency (9.375 GHz).

The almost constant intensity level of the signal, between the aspect angles of -65 and +65°, corresponds to the region with the same scattering level of the reflector, being a characteristic RCS pattern for this target. The obtained RCS pattern shows a good agreement with that one provided by the manufacturer.

Using these data obtained with the Luneberg reflector it is possible to determine the RCS value for other single targets based on equation 9.

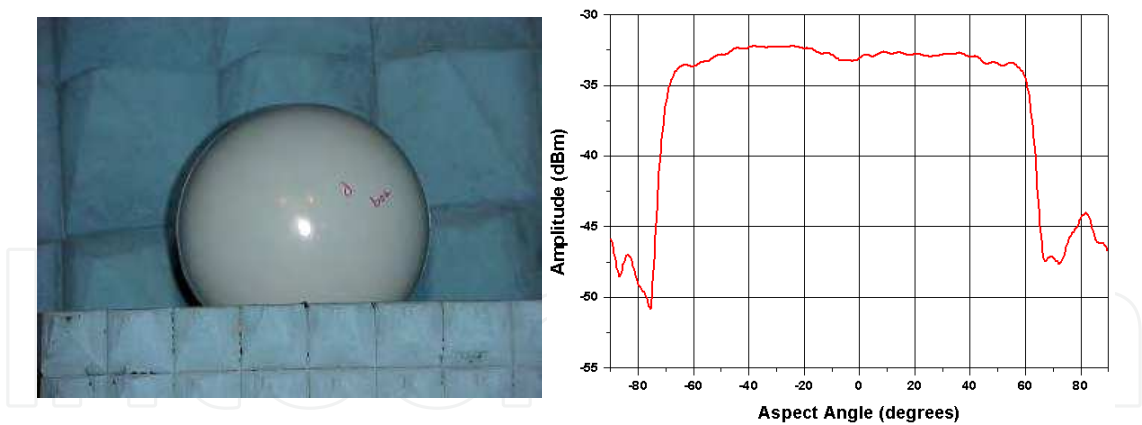


Fig. 9. Luneberg reflector positioned in an anechoic chamber (left) and a measured RCS pattern at 9.375 GHz (right).

4.1.2 Flat plates RCS reduction measurements

The RCS values of a perfect flat rectangular reflector can have its theoretical RCS value calculated as a function of the incident radiation frequency, according to equation depicted in Table 3. The RCS reduction method to evaluate a flat plate requires a double face panel, where one side is used as reflector material (reference) and the other is coated with ERAM. The panel is fixed on a rotating support, which is positioned in front of the receiving and transmitting horns according to the setup described in 3.1. The advantage of this methodology is that it allows the evaluation of the reference and ERAM, by rotating the device from 0 to 360°, evaluating both sides of the panel, one after the other. Figure 10 shows a simplified scheme of the device used in RCS method. With this method, it is not necessary to make two separate measurements, because the RCS pattern of the ERAM is made by rotating the device from 0 to 180° and the reference (metal plate-reflector) is made from 180 to 360°. Thus, it is a self-calibrating measurement (Knott et al., 1993).

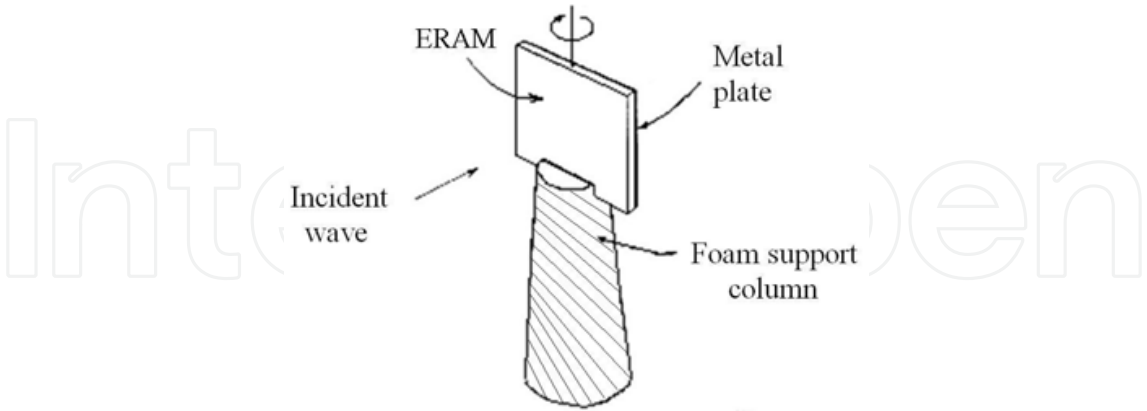


Fig. 10. Device scheme used for the RCS measurements.

The tested ERAM coating was prepared at Materials Division/IAE/DCTA, from Brazil. The ERAM preparation involved the mixture of 60 % (w/w) of a commercial polyurethane matrix loaded with 40 % (w/w) of fillers, being carbonyl iron (20 %) and ferrites of MnZn (10 %), NiZn (5 %) and MgZn (5 %). Physico-chemical characteristics of the fillers and the polyurethane resin as well as the coating preparation procedures were previously described

(Martin, 2002). The ERAM was applied on the aluminum flat panel of 300 mm x 200 mm surface by brushing with thickness of 0.7 to 2.0 mm.

RCS measurements were carried out at the frequency of 8 GHz and the panel (300 mm x 200 mm) was fixed on the rotating support (Figure 11) and rotated from 0 to 360°, at a scanning rate of 0.080 rad/s, characterizing both sides of the panel, i.e., the reference side and the ERAM painted side. From 0 to -180° it is scanned the reference side and from 0 to + 180° the ERAM coated side.



Fig. 11. Flat plate assembled in an anechoic chamber: metal face (left) and ERAM face (right).

Figure 12 shows the RCS pattern of the reference aluminum plate, obtained at 8 GHz, with a rotation of 180°. It is observed a peak at 0° corresponding to values of -25.3 dBm (that results in a RCS value about 32.1 m² using an appropriate reference target), due to the normal incidence of the electromagnetic waves on the reference plate. The position of the plate is a critical point for the success of the measurements, where changes of ± 8°, for example, can change the signal intensity for nearly -35 dBm. This abrupt dropping of the signal for angles different from 0° is due to the flat geometry of the target, scattering the electromagnetic wave impinged on it in different directions of the receiving antenna.

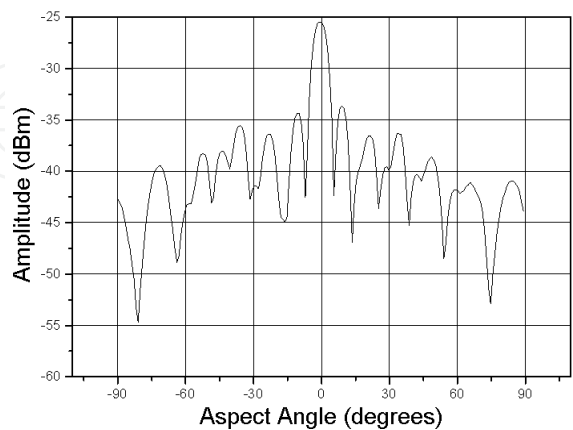


Fig. 12. RCS pattern of an aluminum plate (300 mm x 200 mm), at 8 GHz.

Afterwards, RCS measurements were carried out with the panel having one side coated by ERAM. Figure 13 shows the RCS pattern expressed in dBm and in square meters, both

obtained at 8 GHz. In the range of 0 to -180° it is observed a peak at -90° , corresponding to the normal incidence of the radiation on the reference side of the panel.

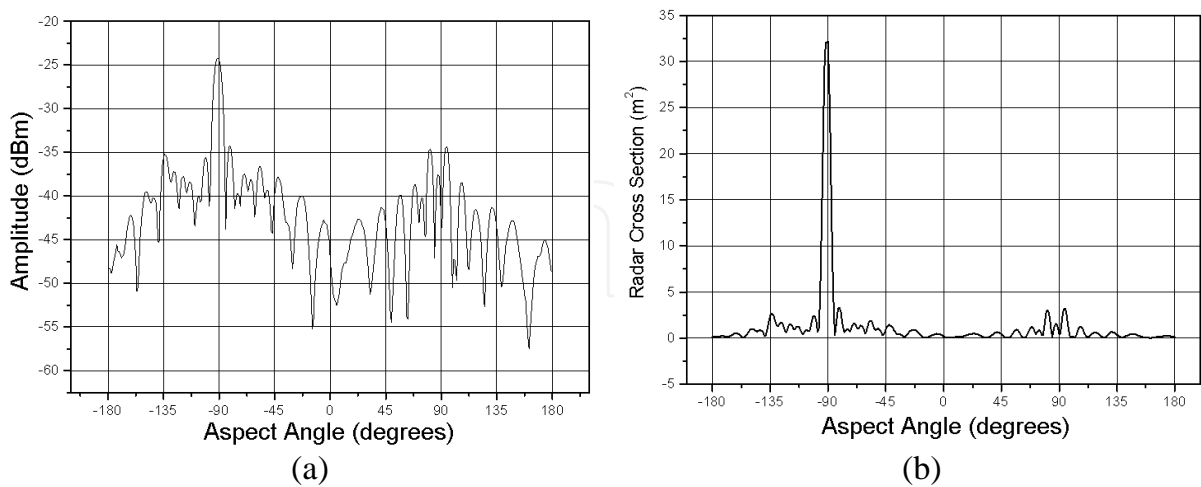


Fig. 13. RCS measurements of the panel (300 mm x 200 mm), at 8 GHz: (a) in dBm and (b) in m^2 . Reference side (-180° to 0°) and ERAM coated side (0° to $+180^\circ$).

The attenuation obtained at the frequency of 8 GHz, presented above, at the incidence angle of 90° is about 10 dB. The measurements showed clearly that the RCS values decrease when the ERAM is applied on the flat plate. The processed ERAM coating is able to attenuate nearly 94 % of the electromagnetic wave, when impinged at 90° , at 8 GHz.

4.1.3 Dihedral and trihedral corner reflectors

Corner reflectors consist in geometries of special interest in electromagnetic scattering problems because they provide a large bistatic or monostatic radar cross section over a broad range of observation and aspect angles. The large echoes from these targets arise from the multiple reflections between two or three mutually orthogonal flat surfaces forming the reflectors. Dihedral corners have been used by many works in RCS reduction studies and also as RCS calibration target (reference target). Trihedral corners yield large backscattering RCS over a wide azimuth and elevation angular ranges and are widely used for external radar calibration.

Both dihedral and trihedral corners are usually present in mechanical structures of ships, aircraft and vehicles, contributing as efficient scattering centers of such targets.

Thus RCS reduction of such geometric corner structures is of great importance in the design and construction of ships and aircraft which will be under surveillance of radar systems. It has been reported that RCS reduction of dihedral corners can be achieved by altering the mutual orthogonality of the flat surfaces. This technique involves changes in original engineering design of the target. Meanwhile, the use of ERAM can also overcome this problem.

This section shows the results involving the RCS reduction of a square dihedral and trihedral corner reflectors, coated with ERAM developed at Materials Division/IAE/DCTA. The characterization was performed using an anechoic chamber in the frequency range of 8 – 12 GHz.

RCS measurements were carried out at the frequencies of 8, 10 e 12 GHz. In each frequency, the dihedral and the trihedral were fixed on the rotating support and rotated from -90° to $+90^\circ$, at a scanning rate of 0.15 rad/s. In this process two pieces were utilized, one as reference and the other coated with the ERAM (previously described). Figure 14 shows the assembly of a dihedral inside the anechoic chamber used in this work.



Fig. 14. Assembly of a dihedral on the azimuth positioner.

Figure 15 shows the results at 10 GHz of the reference dihedral (-180° to 0°) and this target coated with ERAM (0° to $+180^\circ$). The dihedral RCS pattern is characterized by multiple reflections of the wave between the orthogonal faces, with two peaks in the aspect angles of -135° and -45° . These peaks are attributed to the wave normal incidence on the flat side of the dihedral. It can be observed at 10 GHz (Figure 15) an attenuation of nearly 13.6 dB and 10 dB at -135° and -45° , respectively in the RCS pattern of the ERAM coated dihedral, in comparison to the reference one. Between $+45^\circ$ and $+135^\circ$ angles it is verified an attenuation of 20 - 24 dB, attributed to the multiple reflections of the wave between the orthogonal faces of the dihedral.

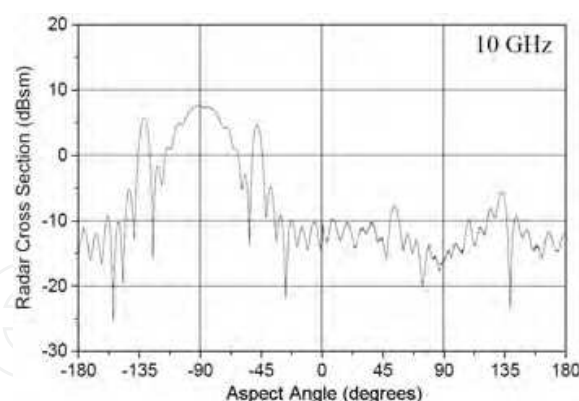


Fig. 15. RCS pattern of a dihedral (120 mm x 120 mm), reference side (-180° to 0°), ERAM coated side (0° to $+180^\circ$).

Figure 16 depicts the results at 8 GHz of both, the reference trihedral (-180° to 0°) and the ERAM coated one (0° to $+180^\circ$). The trihedral RCS pattern is characterized by multiple reflections of the wave among the three faces. In a similar way, the resulted RCS pattern is similar to that one verified for dihedrals. At 8 GHz, the RCS pattern shows a reduction of 17 dB for the ERAM coated trihedral in comparison to the reference one, between the aspect angles of $+45^\circ$ and $+135^\circ$. However, in the angle range of $+135^\circ$ to $+180^\circ$ and 0° to 45° is observed a signal increase related to the reference trihedral.

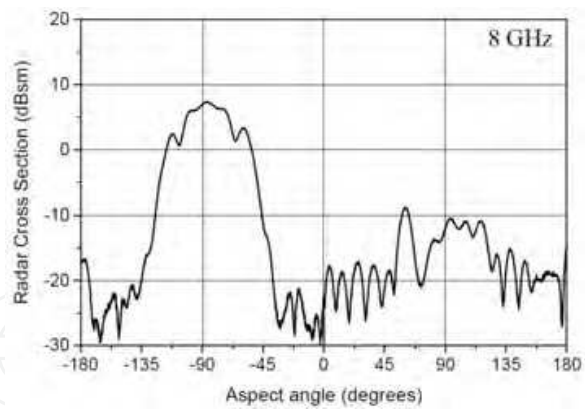


Fig. 16. RCS pattern of a trihedral (120 mm x 120 mm), reference side (-180° to 0°), ERAM coated side (0° to +180°).

4.1.4 Cylinders

The RCS of a metal cylinder has well-known theoretical equations and making use of some considerations, the RCS of a cylinder can be calculated. However, unlike the perfectly conducting sphere, the cylinder is sensitive to wave polarization.

The calculations involving cylinders generally assume that the axial length of the cylinder is large compared to the wavelength. The RCS pattern of a cylinder can be represented by an almost constant value over the entire range of the aspect angle that should, ideally, result in an omnidirectional pattern.

The advantage of using a metal cylinder with a low roughness, as support for testing the reflectivity of ERAM, lies on RCS values nearly constant with the angle of the incident wave. Therefore, the ERAM coated cylinder characterization is more influenced by possible variations of ERAM texture, homogeneity of the absorbing additives distribution and also the absorber thickness. Possible variations of these parameters will result in change of RCS pattern as a function of aspect angle of the incident wave. Figure 17 shows the cylinder mounted on the positioner, located inside an anechoic chamber, uncoated (Figure 17a) and ERAM coated (Figure 17b).

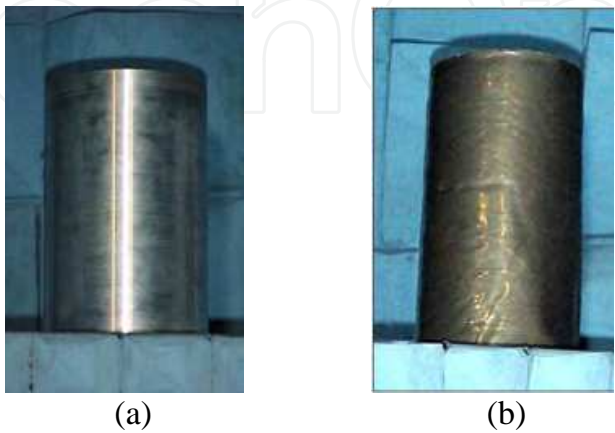


Fig. 17. Assembly of an uncoated (a) and a coated (b) cylinder inside an anechoic chamber for RCS reduction measurements.

Figure 18 depicts the plotted RCS pattern of a metallic cylinder of 32 cm of length and 15 cm of diameter, rotating the cylinder from +90° to -90° on its axes and keeping the TX and RX antennas in the same position, at 9.375 GHz. The determined RCS value is constant and omnidirectional, equal to 1.61 m². The cylinder RCS measurement needs a tight adjusts on the dielectric support to avoid contributions of the reflected waves from this apparatus.

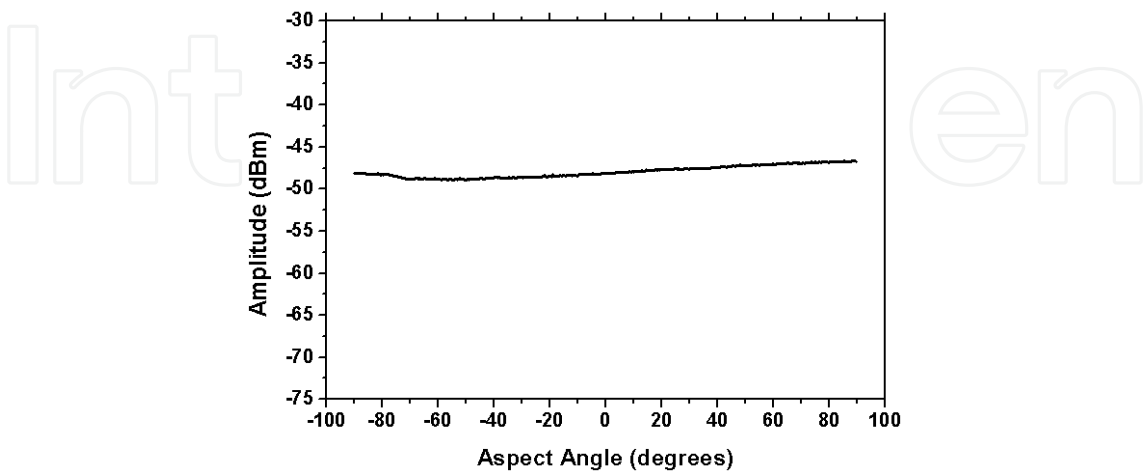


Fig. 18. RCS pattern of a cylinder at 9.375 GHz.

The received power level is almost constant at 9.375 GHz (-49.7 ± 1.0 dBm) rotating the support in 360° around its vertical axe. This curve is typical for this kind of target and it is attributed to the cylinder shape, which contributes only as a line when the wave impinges on it. Afterwards, using the same device and the same cylinder it was obtained the RCS pattern of this target coated with a processed ERAM (Figure 19).

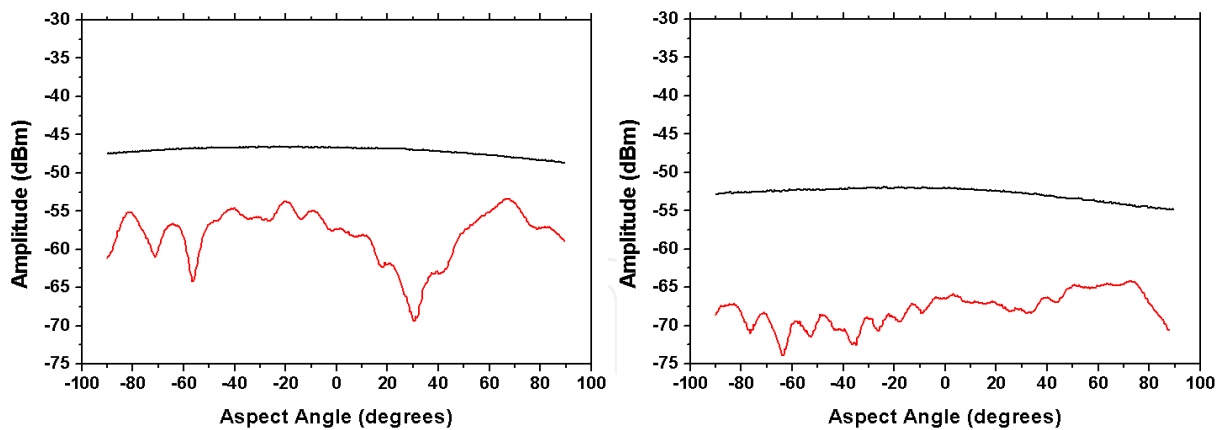


Fig. 19. RCS patterns of cylinder without ERAM (black curve) and coated with ERAM (red curve) at 10 GHz (left) and 12 GHz (right).

Figure 19 shows the RCS pattern of the cylinder at 10 GHz and 12 GHz coated with the ERAM presenting 1.2 mm of thickness loaded with NiZn ferrite and carbon black. In this case, the pattern shows the reflectivity variation in function of the aspect angles, characterizing a RCS reduction of the target. This variation is attributed to the heterogeneity of the processed ERAM, related to both the ferrite and carbon black particles distribution and the absorber thickness.

4.2 Complex shapes targets

The total RCS of a target of complex geometry can be determined by various techniques of different levels of complexity. One approach involves dividing the object into several parts, and these should approach targets of simple geometry. The determination of the RCS of each of these parts, the sum of their individual contributions to the total reflected field, taking into account their respective phase angles and reflectivity, provide the final value of the target RCS of complex geometry.

A complex target has multiple scatters interacting with each other, changing the RCS as a function of aspect angle. For those targets, the peaks of RCS pattern may be many wavelengths apart, but they can add up constructively or destructively by a fraction of degree.

The RCS pattern of a complex target is a function of many variables in the radar system and environmental measures. In addition to the change in aspect angle and shape of the target, there are multipath and atmospheric effects. The main reflection mechanisms of a complex object are: specular reflection, surface waves, edges diffraction and cavities.

In the next section will be treated the RCS studies of complex targets (mainly missiles) done by the Materials Division/IAE/DCTA from Brazil.

4.2.1 Missiles

Missiles possess one of the most fundamental complex geometries to RCS prediction and electromagnetic characterization. These ones present a relatively simple geometry in comparison with more elaborate targets, such as aircraft and ships. However, these shapes allow detailed studies of the scattering phenomenon of the simple geometries that constitute them (Ruck, 1970). In this section, it is shown some RCS results achieved in the characterization of a hypothetical missile and a real missile section, in the microwave range of 5 to 7 GHz. ERAM application on the studied targets is also evaluated.

4.2.1.1 Characterization of a hypothetical missile in indoor measurements in C-band

A prototype was projected and constructed and called 'hypothetical missile'. The purpose is to understand the behavior of an actual complex target, from the well known physical and mechanical characteristics of a prototype. The dimensions of the hypothetical missile correspond to those of a cylinder measuring 0.32 m x 0.15 m and four square flat plates measuring 0.15 m sideways.

The study presented in this section intends to compare the results obtained experimentally with data obtained theoretically, by predictions based on literature (Knott, 1993). An algorithm to simulate the radar signature of complex geometry was developed with the purpose of both estimating the contributions of each simple component of the target and assisting the analyses of the experimental measurements (Miacci, 2006).

The foreseen aspect, by simulation, of the RCS pattern for this type of target is shown in Figure 20. This figure demonstrates the appearance of the peaks relative to the frontal, back and sides contributions of the target. Figure 20 shows also a view inside the anechoic chamber, where the system was assembled for the RCS experimental measurements for the frequency range of 5.8 to 6.4 GHz.

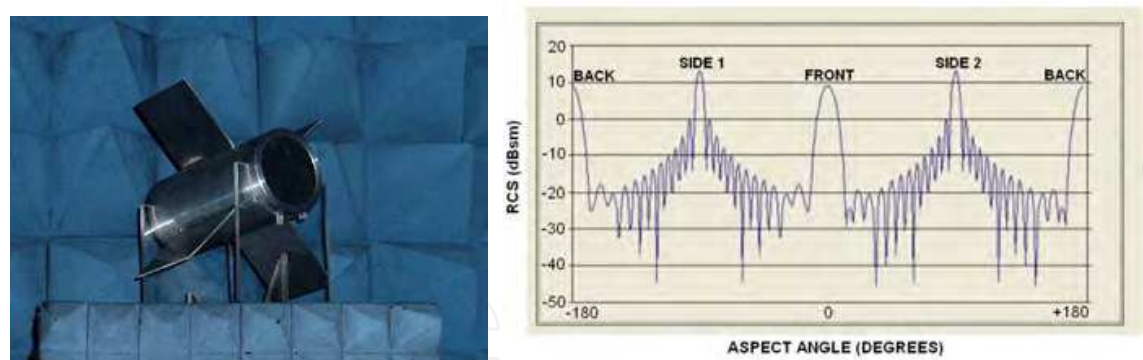


Fig. 20. Simulated RCS pattern for the Hypothetic Missile at 6.0 GHz and the Hypothetic Missile placed in the anechoic chamber.

The same missile was placed in the anechoic chamber and characterized in accordance with the procedures and the RCS patterns obtained at frequencies 6.0 GHz and 6.4 GHz are shown in Figure 21. Comparing Figures 20 and 21 good agreements of the patterns is verified. However, the figures relative to the experimental measurements show less detailing of the secondary lobes. From these patterns, the RCS values can be calculated for the hypothetical missile, as shown in Table 4.

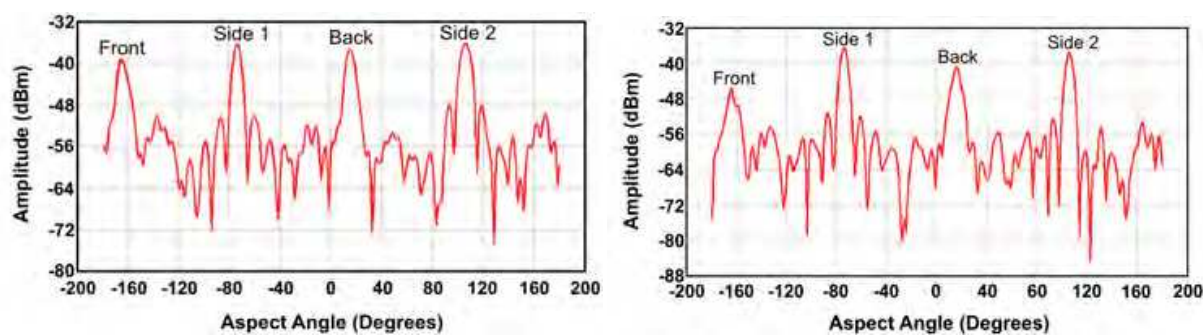


Fig. 21. RCS pattern measured from the Hypothetic Missile at 6.0 GHz (left) and 6.4 GHz (right).

Frequency (GHz)	RCS maximum (dBsm)
5.9	09.2
6.0	11.5
6.2	11.9
6.4	13.0

Table 4. Experimental RCS Values of the Hypothetical Missile (deviation: 0.7 dB).

The analysis of Table 4 shows the maximum RCS variation of the hypothetical missile (9.2 – 13.0 dBsm) as a function of frequency, hence evidencing the sensibility of this measure with small variations on the wavelength of incident radiation. From such measurements it can be affirmed that the system is reliable to accomplish RCS measurements of complex geometry targets.

4.2.1.2 RCS reduction of the hypothetical missile

Reflectivity measurements of the Hypothetical Missile coated with ERAM were performed (Figure 22) and the results were compared with those presented in preceding section. In

order to improve the evaluation of the ERAM effect on the Hypothetical Missile, this material was applied in only a portion of this target under test, i.e., a face of the missile was not covered with the absorber. Thus, we applied the ERAM on the front and over one side, while the rear and the other side did not have their surfaces coated (Figure 23).



Fig. 22. View of the Hypothetical Missile with applying of ERAM.

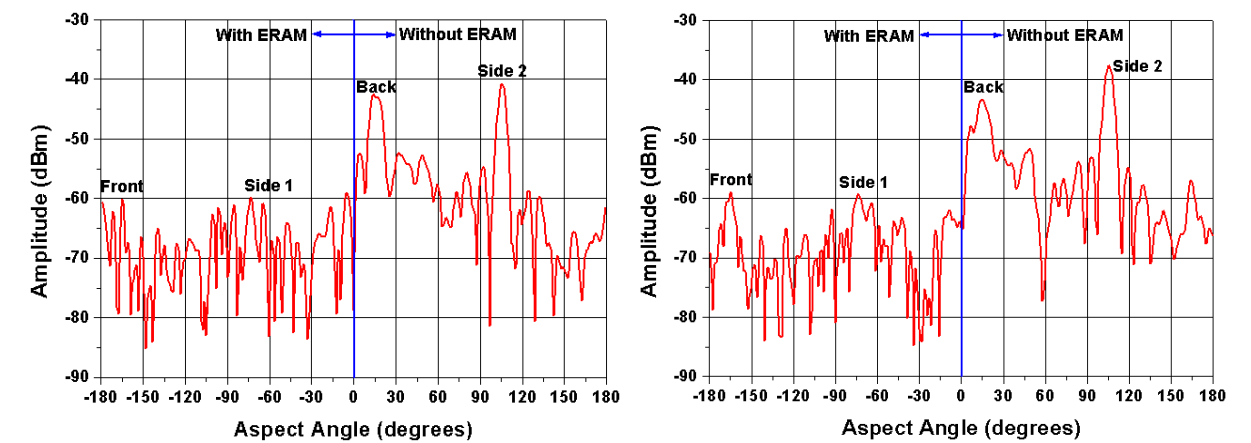


Fig. 23. Reflectivity curve of the Hypothetical Missile partially covered with ERAM, at 6.2 GHz (left) and 6.4 GHz (right).

Table 5 shows the results and compares the RCS reductions achieved.

Frequency (GHz)	RCS Reduction (dB)	Measured RCS (dBsm)
5.9	16	-6.8
6.0	19	-7.5
6.2	19	-7.1
6.4	21	-8.0

Table 5. RCS reduction with the ERAM on the Hypothetical Missile (deviation: 0.7 dB).

The analysis of Table 5 shows that the RCS reduction values (16 - 21 dB) are in accordance with the attenuation values of the used ERAM (~ 20 dB attenuation). This behavior shows that the proposed experimental method is effective for the study of RCS reduction of complex geometries. The main contributions are highlighted in the figures.

4.2.1.3 Characterization of a missile's section in indoor range in C-band

After verifying the reliability of the parameters adopted in the employed methodology, the characterization of the actual complex target was performed. For this, the selected section of the actual missile was placed in the anechoic chamber (Figure 24). The results obtained in the reflectivity measurements are illustrated in Figure 25.

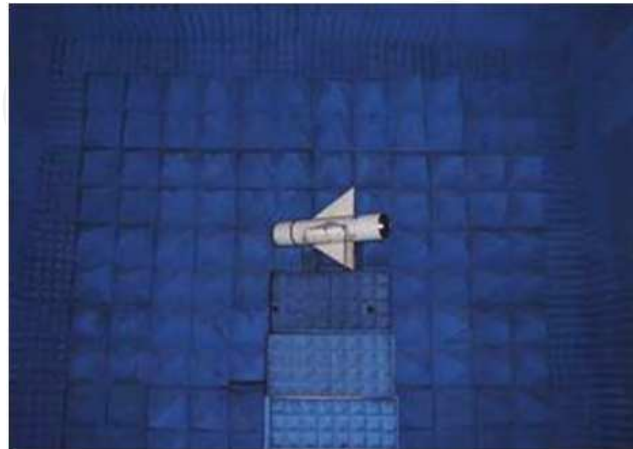


Fig. 24. View of the missile's section positioned in the anechoic chamber.

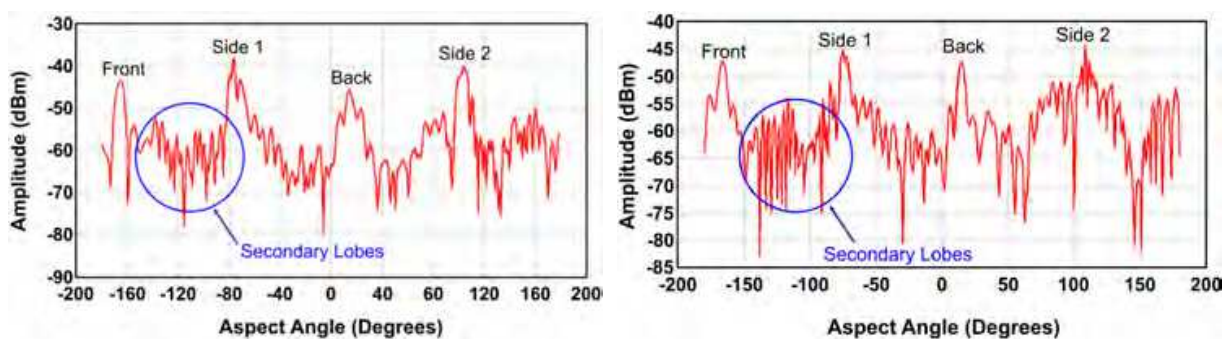


Fig. 25. RCS patterns of the missile's section at 6.0 GHz (left) and 6.4 GHz (right).

Figure 25 represent the obtained curves that are typical of the reflectivity patterns of the missile's section characterized in the anechoic chamber at a frequency range of 5.9 to 6.4 GHz. The comparison of these figures shows that the frequency increase is accompanied by greater detailing of the patterns. This behavior shows a larger contribution of the secondary lobes. These figures reveal also the real complexity of the RCS patterns of complex targets.

The results of these measurements suggest the presence of phenomena commonly seen in experiments performed with this type of geometry. As the missile's section presents similar geometry to that one observed in the hypothetical missile, it is expected that its pattern adjust adequately to those measured for the hypothetical missile.

However, the presences of triangular-shaped flat plates (the missile's warp) and the irregular aspect of the surface contribute with new peaks, increasing the complexity of the pattern. Besides the front part of the missile is not a perfect flat plate, since before this area has the boundary with the tracking compartment, modifying the outline of this target's reflectivity pattern, contributing also to the complexity of the RCS pattern.

Another phenomenon observed is with regard to the non-symmetry of the pattern between the angles of -180 to 0° and 0 to $+180^\circ$, which reveal peaks of different shapes and amplitudes. This is due to the contributions of physical details of the missile, such as compartments of electronic circuits, conduits where the cables pass through and connectors integrated to the cylindrical body of the target.

Such devices positioned on the missile’s body, which at first seem to be of little influence, cause wave scattering on the target’s surface, which alter the reflection as a whole, such as diffraction edges and traveling waves. These constructive attributes of the missile are displayed in the measurements and results in alterations in the pattern peaks. These results justify the complexity of the reduction of the target’s RCS of complex geometry, as foreseen in literature (Ufimtsev, 1996).

The measured RCS values for these cases can be seen in Table 6.

Frequency (GHz)	Maximum RCS (dBsm)
5.9	7.3
6.0	7.9
6.2	10.2
6.4	10.5

Table 6. Experimental RCS values for the missile’s section (deviation: 0.7 dB).

4.2.1.4 RCS reduction of a missile’s section

ERAM was used covering selected faces of the missile, i.e., the faces covered and uncovered resulted in a pattern for direct comparison of RCS reduction. Analogously to make with the hypothetical missile, ERAM was applied on the front part and on one side, while the rear and the other side remained uncoated (Figure 26). Figure 27 show the RCS reduction patterns obtained at 6.0 and 6.4 GHz.

Similarly to that observed in the Hypothetical Missile measurements, it is verified the RCS reduction of the faces with ERAM. In a similar way, the application of ERAM promotes attenuation values of the target’s RCS close to those determined for the ERAM (~ 20 dB). Table 7 shows the reduction obtained in this case.



Fig. 26. View of the missile’s section covered with ERAM.

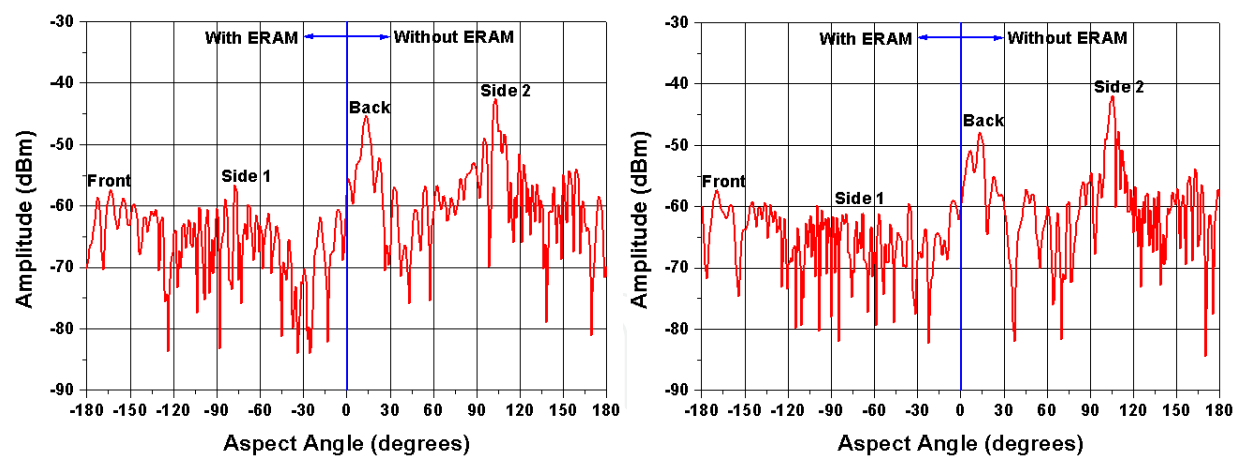


Fig. 27. Reflectivity curve of the missile’s section partially covered with ERAM at 6.0 GHz (left) and 6.4 GHz (right).

Frequency (GHz)	RCS Reduction (dB)	Measured RCS (dBsm)
5.9	11.5	-4.2
6.0	14.0	-6.1
6.2	18.5	-8.3
6.4	18.0	-7.5

Table 7. RCS reduction of the missile’s section coated with ERAM (deviation: 0.7 dB).

5. Conclusions

This work shows a reliable methodology for RCS measurements of simple and complex targets. Indoor RCS measurements of simple and complex targets in C and X-band are explored and the results show good agreement with the literature. Reflectivity measurements of the studied targets coated with electromagnetic radiation absorbing materials demonstrate that the proposed measurement system is satisfactory for RCS reduction studies.

This work presents also, results of an active cancellation circuit as an enhancement technique for the RCS measurements. The proposed circuit increases the detection probability of smaller targets, associated with a greater dynamic range of the measurement system. Therefore, the proposed circuit makes the study of RCS reduction more effective concerning small targets covered with high attenuation ERAM. An increase of dynamic range of up to 26 dB at 5.9 GHz frequency is observed. Consequently, the minimum detectable RCS values using the proposed circuit increased significantly, as for instance -9.0 dBsm (without the circuit) up to -35 dBsm (with the circuit) at 5.9 GHz.

The recovering of any targets with a determined ERAM developed at Materials Division/IAE/DCTA in Brazil it was possible to compare and to discuss the influence of the ERAM on the observed RCS reduction. The used methodology showed useful for attending aeronautical and telecommunication applications.

For the first time in Brazil, the RCS of missile’s sections (hypothetical missile and an actual missile section) was experimentally determined, in C-band in an anechoic chamber.

The evaluated RCS measurement system proved to be effective, with measured values within the expected error range (lower than 1 dB). The obtained results enable to conclude that this methodology is applicable in the characterization of various types of simple and complex geometry targets in indoor and outdoor ranges, attending the far-field condition. In function of the results obtained, employing the presented system, further in-depth studies of RCS reduction is feasible for other military platforms, given its functionality.

6. Acknowledgment

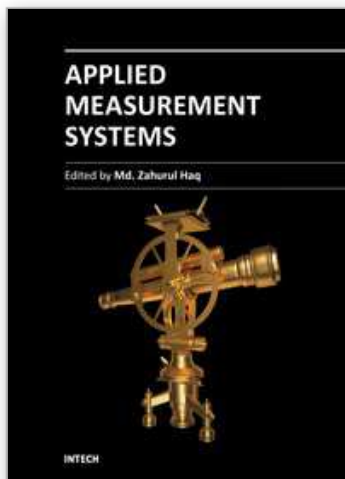
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