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Reconfigurable Antennas of Wide Tuning Ranges and Controllable Selectivity Using Matching Networks

Chin-Lung Yang and Chieh-Sen Li

*Department of Electrical Engineering, National Cheng Kung University
Taiwan*

1. Introduction

In this chapter, a novel design method was proposed for reconfigurable antennas, independent of the geometries and the dimensions of the antennas, providing wide tuning ranges and controllable selectivity. A simple, unspecified S-UWB antenna can be attached to a feeding network to form one integrated selective and reconfigurable antenna. Through the design of tunable wideband matching network, a simple modified ultra-wide band (UWB) antenna can be reconfigurable and re-operated in different bands over a wide of ranges. Based on UWB antennas with proper T- or π -shaped matching network designed in frequency domain, the receiving antennas can be switched to specific bands or even multiple bands continuously. Most of the multiband antennas need complicated approaches to control bandwidths and lack of tuning flexibility. However, the design principles and the controlling mechanism based on microwave circuit theorems are relatively simple, so different fractional bandwidths from 5% to 20% can be feasibly implemented in our proposed architecture. Therefore, the parameters for the antenna operation bands and bandwidths can be calculated and estimated in a straight forward manner.

The L-, T- and π -network are chosen for examples to demonstrate the performance in simulation and in implementation. The simulation results show that the proposed antenna can cover from 1.8 GHz to 11.5 GHz with bandwidth ~ 300 MHz. Replacing the L- type with a T-type or π -type network which gives one more variable freedom to achieve high selective reconfigurable antenna of 80 MHz bandwidth. By utilizing special designed tuning inductors, the antenna bandwidth can be further controllable. The simulation results show that this proposed antenna can switch to 1.8, 2.45, and 3.5 GHz with bandwidths from 80 to 400 MHz.

The proposed antenna architecture provides a reconfigurable RF front end for transmission and reception. Such high flexibility can enable antennas to operate in varying environments for biomedical applications and different bands and thereby, make antennas applicable to wireless body area network (WBAN) as well as multi-mode/multi-band commercial applications. The novel circuitry antenna (modified UWB antenna combining with feed matching components) approach expands the flexibility and the bandwidth for multiband communication systems in a simple implementation.

Reconfigurable multi-band antennas have drawn attentions for modern heterogeneous communication systems, such as antennas for quad-band cellphones, Software-defined

radio (SDR), and Cognitive Radio (CR) which even requires antennas to cover multiple bands or operate at flexible frequency ranges. New technologies, such as micro-electromechanical systems (MEMS), expand the reconfigurable design varieties [Weedon 1999]. In this chapter, a novel concept of ‘impedance matching in frequency domain’ (as Figure 1) is proposed to make the design of reconfigurable antenna straight forward and can be implemented in low cost, simple circuits. This method is different from other methods based on the geometric modification which is developed to induce multiple resonant radiating frequencies. For example, the tri-band antenna is constructed based on a patch antenna design [Guo 2008][Sheta 2008] which peels off some slots or connect some discrete patches to create other effective current path and enable higher/lower radiation frequencies. Most of the designs modify the geometries and the dimensions of the antennas for multiband antennas. Moreover, this seems similar to but is totally different from filter-based reconfiguration. The most obvious feature is that it is not easy for tunable filters to design and implement, nor is its bandwidth tuning easily. In our proposed architecture, merely three components can fulfill reconfigurable antennas of wide tuning ranges and controllable selectivity by using matching networks.

A tunable filter provides an excellent selection to implement tunable bands, but tunable filter are usually difficult to design and control. The comparison is listed in Table 1. To achieve tunable capability, our proposed architecture has advantage of very wide tuning range, flexible control, and easy analysis. There are currently many fabrication technologies [Hoarau 2008]. Hybrid circuits using discrete components such as diodes and SMD components are easier to make and design for prototypes in commercial bands to verify concepts, and these components may be further integrated in compact size in the future. The main design issues of tunable matching network include applicable frequency ranges, impedance tuner dynamic range, control methods, linearity, size and losses. Concerning the tunable frequency range, a high selectivity usually comes along with a limited tunable range. However, this problem can be easily overcome in our proposed architecture. The four main investigative objectives in this chapter are operating frequency ranges, other undesired bands suppression, the use of one single component to fulfill the tunable function, and energy loss reduction.

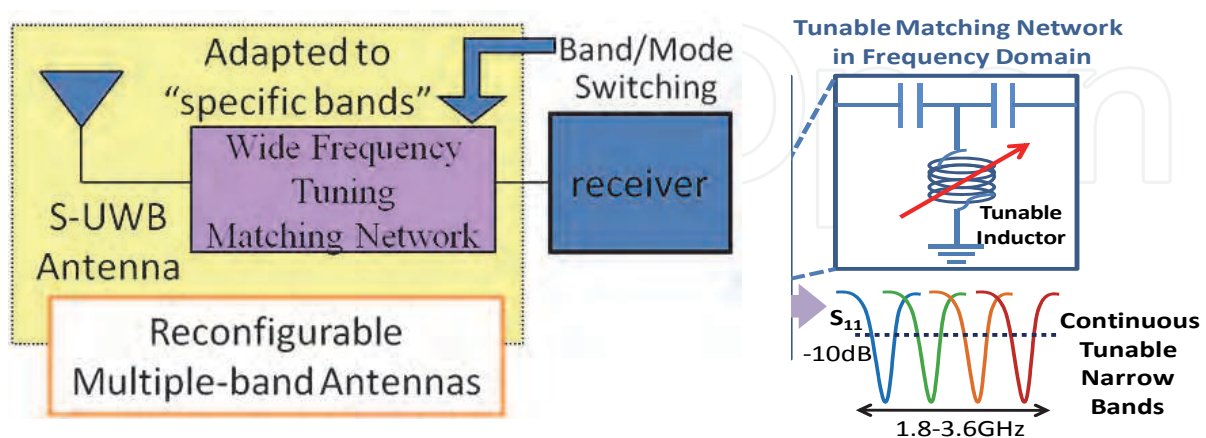


Fig. 1. The architecture of the reconfigurable multiband antennas.

In this chapter, by expanding the concept of “analog antenna” and ‘impedance matching in frequency domain’ [Yang 2009], the design of reconfigurable multimode and multiband

antennas is developed in a straight forward manner and also implemented in low cost, simple circuits. The “analog antenna” in this chapter means that one un-designed antenna combined with a small circuitry to enhance or expand the original function or specification. For this proposed antenna, a frequency-tuning matching network which may have different architectures is added. The illustration of the reconfigurable multiband analog antenna is shown in Figure 1. The matching networks may have traditional structures, such as L/T/ π -shaped matching network and cascaded/mixed matching network with RF switches or varactors to tune the impedance of the semi-ultra wide band (S-UWB) antennas in specific bands, which are easy to design and implement instead of using wide-band reconfigurable and sharp filters. Therefore, multiband can be achieved while covered range is still wide.

Tuning Types	Tuning		Analysis	Impedance Matching	Antenna Patterns
	Range	Control			
Modified Geometry	Broad	+++	Middle	Yes	Yes
Tunable Filter	Narrow	+	Hard	No	No
This Design	VeryWide	++++	Easy	Yes	No

Table 1. Typical Comparison for Frequency Tuning Functions

Moreover, to add on extra specific bands needs not to re-design the whole antenna, but to modify the matching network parameters. In this chapter, we demonstrate this concept in tri-band using lump elements for the prototypes. ADS simulations are performed to predict those multiple bands and procedures of tuning these practical lumped component values are also developed and will be addressed later. The proposed switchable multi-band antennas have the features of utilizing semi-UWB antennas, operating at multiple bands, re-configuration, and controllable bandwidth. However, these multiple bands will not occur at the sample time, each one will function as the communication system switches to their mode and frequency.

2. System description and design principles

This system includes three parts: a semi-UWB antenna, frequency-tuning matching network, and the controlling unit. The system block is shown in Figure. 2. From this figure, not only the components are variable, but also some switches are placed at the joins of the matching network to modify its own architectures. Two major steps for such proposed multiband antennas include S-UWB antenna design and matching network design. The controlling unit is assumed to be pre-assigned to turn on different modes. Each step is easy and quick, so the development and optimization process can and be improved significantly. In this chapter, a tri-band system will be demonstrated and operated at 1.8 GHz, 2.45 GHz, and 3.5 GHz, which are common for cellphone frequency band (GSM), ISM/WLAN band, and WiMAX band in some countries, respectively.

Taking loss and design complexity into consideration, we use as few components as possible to simplify mathematical analysis and induce less loss. In contrast to L-type network which has limited impedance dynamic ranges to match and lack of freedom for controllable Q value, T-type and π -type networks are commonly confined to carry out high selectivity and

a wide scope of tunable impedance network due to that the extra degree of freedom can further be used to control the bandwidth. We chose a T-type (C-L-C) network that includes two serial capacitors and a parallel inductor between them shown as Figure 3. The central shunt part is the variable inductor L, implemented by a fixed L and a varactor.

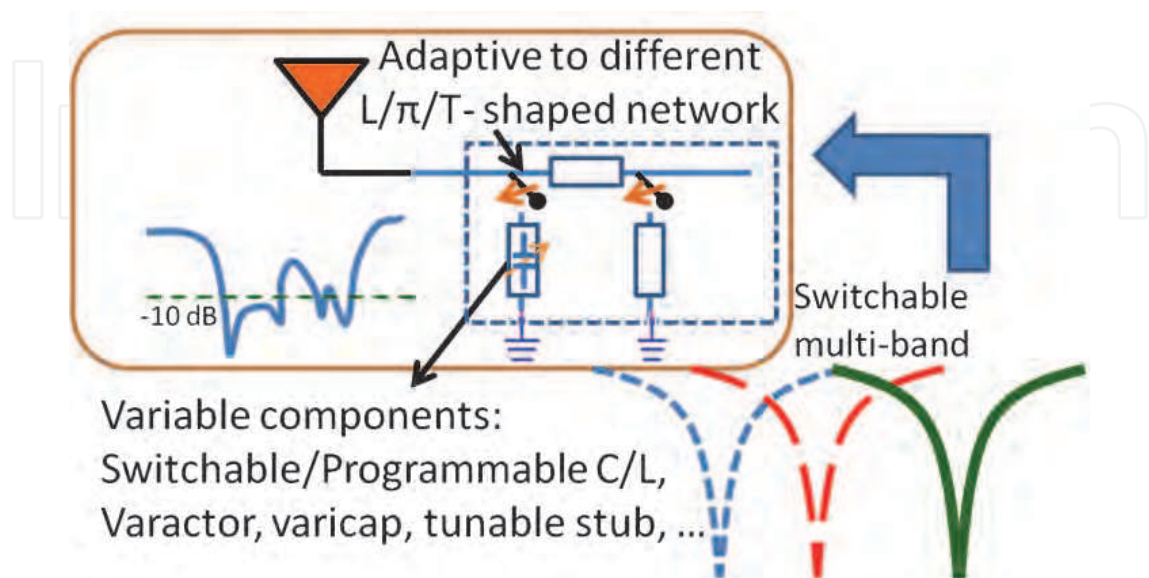


Fig. 2. System diagram of the band-switchable antennas.

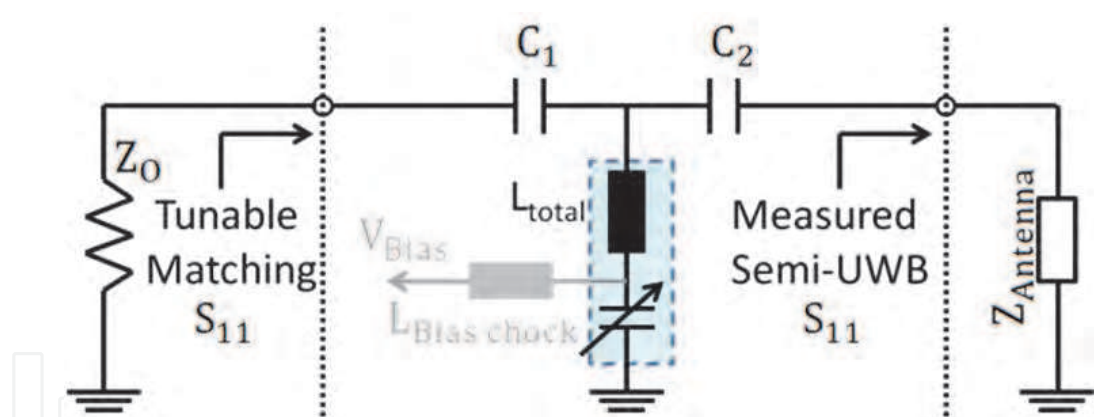


Fig. 3. Equivalent circuit of the tunable matching network and S-UWB antenna with control bias voltages V_{BIAS} , series capacitor shunt inductor L and varactor

There are two major steps to design the proposed reconfigurable antenna, including S-UWB antenna design and tunable matching network design. Each step is quite straight forward and thereby improves significantly the development and optimization process.

2.1 Design for semi-UWB antenna

Instead of designing a tri-band antenna directly to cover these bands simultaneously, a semi-UWB antenna is desired to cover these bands. A semi-UWB antenna means similar to UWB antenna, but it does not guarantee all the return loss below -10 dB over its operation bandwidth. Popular or compact UWB antenna designs can be referred and guided [Wong 2005] [Peyrot-Solis 2005]; however, it is not necessary to optimize all the dimensions to have

ultra wide band response, like one real UWB antenna does (so we called such antennas as S-UWB antennas). On the contrary, radiating over semi-wide bands is sufficient. Therefore, antenna design and procedure for tradeoff between the bandwidth, gain, and efficiency can be reduced substantially.

We randomly pick up two kinds of antennas to demonstrate our concepts and design. One is circle-shaped, and the other is beveled-shaped. A circle-shaped antenna on a 1.6-mm FR4 ($\epsilon_r = 4.3$, loss tangent $\delta = 0.015$) substrate is chosen as one of the options for demonstration in this chapter. Its dimension is determined from HFSS simulations. The relevant dimensions of circular-shape antennas are $[r/d/g/w_f] = 21.3/1/10/2.7$ mm; $[L_1/L_2/W] = 62/19/64$ mm. The dimension of the beveled-shaped one is determined from HFSS simulations and listed in below. The geometry and dimension is shown in Figure 4 and 5. Surely other shapes and UWB-like antennas can be possible to apply following the same design principles. The return loss is measured and shown in Figure 4 and 5. From the result of the measured S_{11} , we found this S-UWB antenna performs relatively poorly at 4-5 GHz, but we need not to tune its dimensions and feeding structure to optimize this antenna. These performances at desired bands will be considered with matching network altogether.

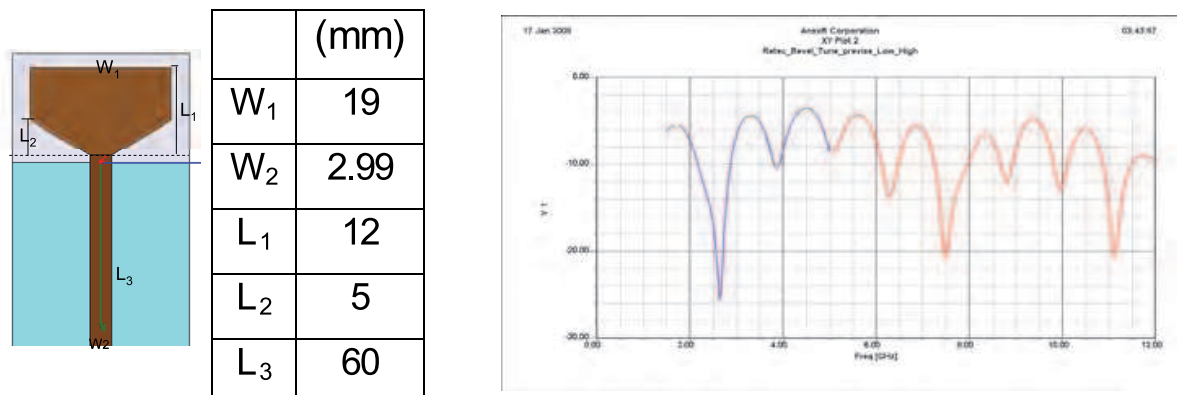


Fig. 4. Beveled-shaped S-UWB antenna and S_{11} plot from the HFSS simulation.

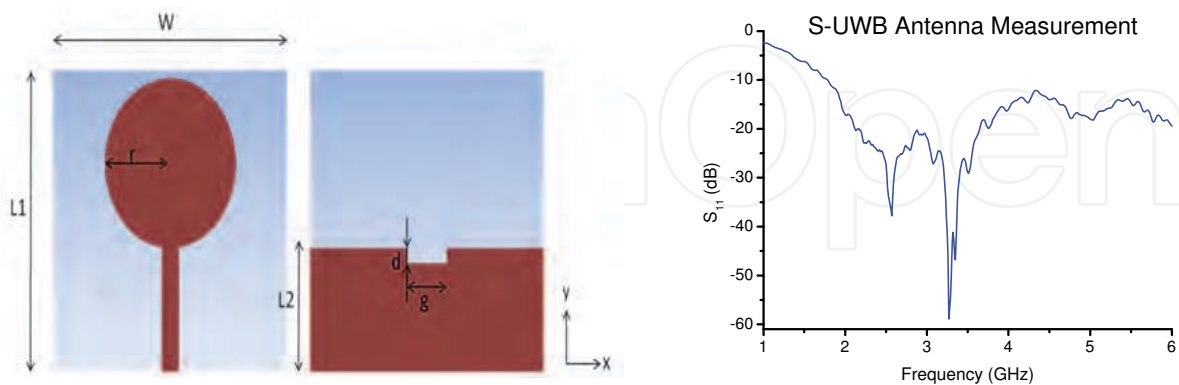


Fig. 5. The circle-shaped S-UWB antenna and S_{11} plot from the HFSS simulation.

2.2 Design for frequency-tuning matching network

The L-C type matching network, which is optional, is chosen to adapt the impedance to match at the desired frequency. Therefore, the overall antenna with the matching network

becomes narrowband band implying high selectivity. This is reasonable due to the semi-UWB antenna has low-Q and overall the response is dominated by the matching network as well. The S_{11} parameters are estimated from HFSS simulations and output as a file to ADS (Advance Design System), so ADS can do the matching network corresponding to the specific S_{11} at target frequencies as shown in Figure 6. After matching network, the S_{11} is re-shaped and a specific frequency can be well-matched as Figure 7(b) shows.

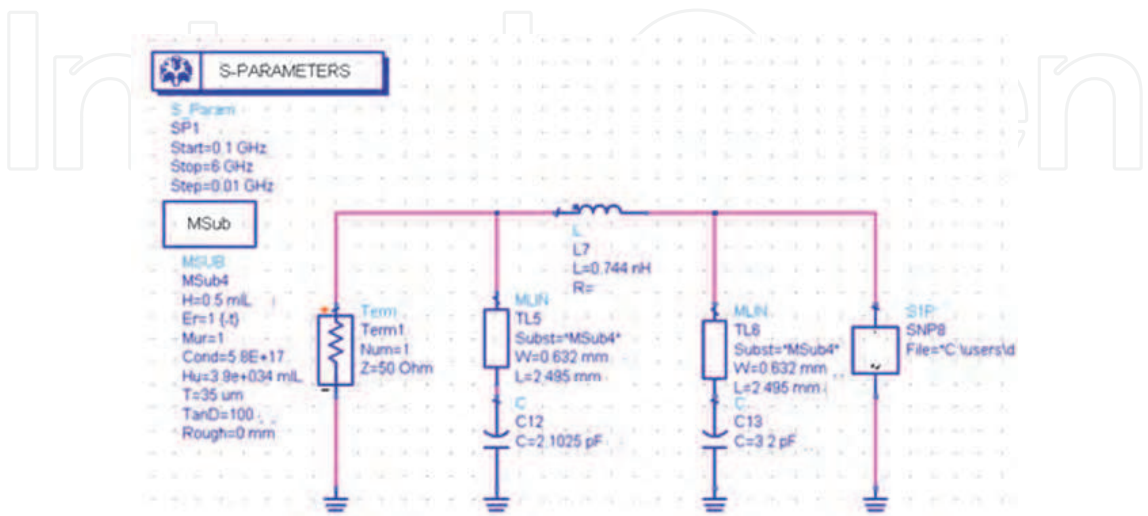


Fig. 6. ADS simulation combined tunable matching network and an S-UWB antenna (S1P).

The π -shaped matching network, which is optional, is chosen to adapt the S-UWB antenna impedance to match at the desired bands. As parts of the L/C components are tunable, this combined analog antenna becomes switchable to specific bands. This is desirable, so the bottleneck of the design of such analog antennas is the tuning and implementation of the matching network circuits which is relative low cost and technically feasible without the modification of the antenna itself. The development starts from the theoretical prediction of the proper L/C component values by feeding the measured S_{11} parameters estimated from HFSS simulations as a load file to Advance Design System (ADS) in Figure 6.

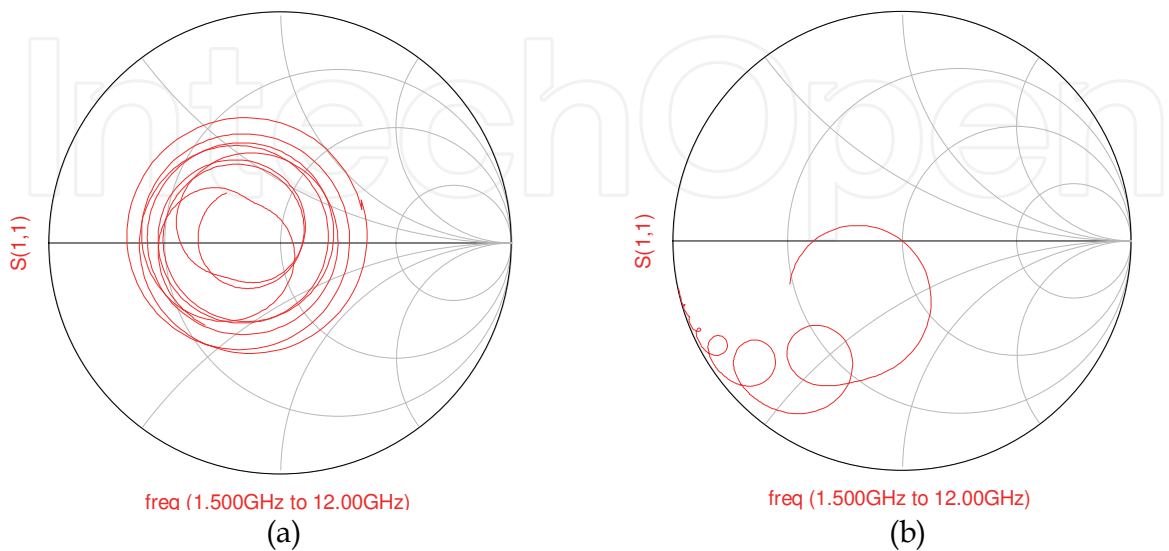


Fig. 7. S_{11} of Bevelled antenna (a) without and (b) with a matching network.

The procedure of determining the component values is shown as below. This is well-established and makes the development of the multiband based on our proposed architecture relatively easy. We further apply a practical C model (S parameters are measured) into the ADS for a fine tuning in the frequency band to reduce the errors of the implementation. Our goal is to set the S-UWB antenna to have good matching ($Z_{in}(\omega_c) = R_s$) at the operation band centered at ω_c , which means $\Gamma_{in}(\omega_c) = 0$; meanwhile we also estimate the bandwidth by circuit Q values. We set a redundant resistance (R_v) as the mediate step to calculate matching as two cascaded L-shaped networks (shown in Figure 8).

$$Q_1 = \sqrt{\frac{R_s}{R_v} - 1}$$

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(1)

$$Q_2 = \sqrt{\frac{1}{R_v - G_L} - 1}$$

(2)

The unloaded Q of the cascaded network $Q = \max(|Q_1|, |Q_2|)$, and the bandwidth can be determined by $2/|Q|$. Applying (1) and (2) into ADS, Table 2 lists the component values of the matching network for this proposed tri-band antenna.

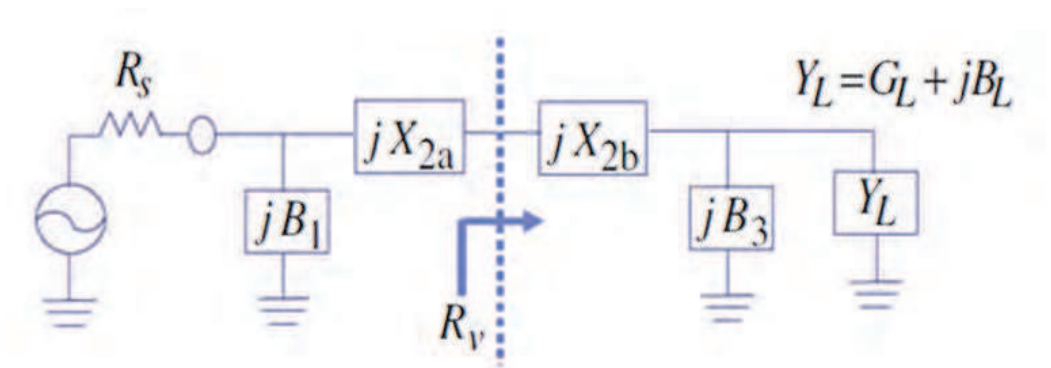


Fig. 8. The mediate step reconfigurable multiband analog antennas.

Frequency (GHz)		C ₁ (pF)	L ₂ (nH)	C ₃ (pF)
Band I	1.8	3.858	2.590	6.545
Band II	2.4	3.760	2.972	5.250
Band III	3.5	2.490	1.150	5.800

Table 2. L-C values of the matching network for tri-band.

According to those desired L/C values based on specific Q values, ADS can fulfill the simulations of this analog antenna at target bands. After π -shaped matching network, the simulated S_{11} of this circular S-UWB antenna is re-shaped to a narrow band antenna and in this specific band, S_{11} can be well-matched as Figure 9 shows. The original S-UWB antenna covers from 2 to 4.5 GHz well. Using the band II parameters, the 2.45 GHz band is will matched, while others are rejected and this proposed antenna functions as a high selective antenna. After the proper L/C values are found, we need further to calibrate the practical values and the influences of the switches (GaAs SPDT, model no. SKY13306-313LF) on the

matching performance for the implementation which will be discussed in the later section. The switches are modeled as loss transmission lines unless they are RF-MEMS switches which provide extremely low loss and huge isolation.

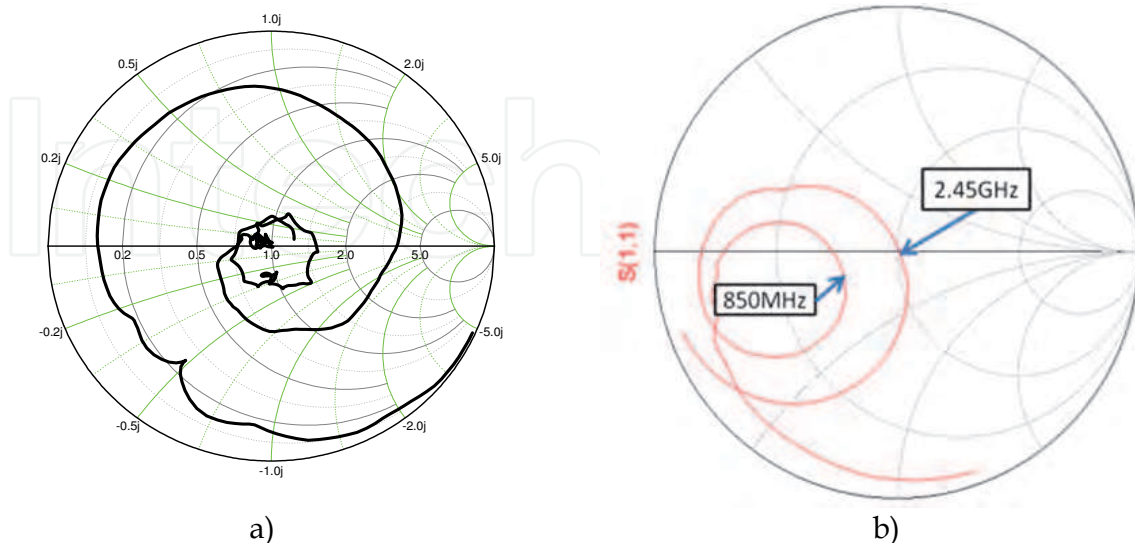


Fig. 9. Measured S_{11} smith chart of circular S-UWB antenna: (a) without and (b) with a matching network tuned to 2.45 GHz.

3. Analysis and simulations for matching network

A complete impedance matching theory and numerical analysis are well-established [Thompson 1996][Schmidt 2007]. However, there exists a high complexity and practical performance loss after considering the parasitic effects, fabrication errors and self-resonant frequency from components in realistic operation. The traditional matching network encounters unavoidable tolerance errors from capacitance and inductance resulting in a frequency deviation away from desired frequency. In this chapter, not only do we have to solve the matching problem, but furthermore, we also eliminate the frequency deviation due to the drifting of capacitance and inductance components.

The Π - and T-type networks themselves can be designed with a desired Q value. However, one common problem for the wideband matching is that uniqueness of the matched bands, which means other undesired bands might happen to be matched unintentionally. Moreover, an unfavorable drawback occurs when using a varactor which needs an additional biased from microstrip line, resulting in discontinuity and parasitic effects. All of these factors above shall be taken into consideration seriously to increase the selectivity and performance. These issues will be addressed in following sections to further improve a highly selective matching network with high Q value and with a continuously smooth tuning effect. These practical factors are also taken into account for simulation, especially for the models of precise values in high frequency.

3.1 Analysis for High-Q tunable S-UWB antennas

One of the unique merits for UWB antennas to design such tunable matching network is that its input impedance already resembles $50\ \Omega$ ($Z_{ANT} \cong Z_0$) within a very broad bandwidth. Based on this characteristic, $50\ \Omega$ terminals are used at both ports of the matching network as the preliminary design to determine the appropriate values of C_1 , C_2 , and L , and to

reduce the number of variables from antenna impedances. We chose two fixed similar low-value capacitors C_1 and C_2 for two serial components of T-type network in Figure 3. The simulation and implementation has proved that this nearly $50\ \Omega$ assumption does not affect the accuracy of performance evaluation.

The high selectivity can be explained by tracing the trajectory of the impedance. By using the first series low-value capacitor C_2 , original antenna impedance, Z_{ANT} , will be moved to the right half of Smith chart (Z_2 , high capacitive reactance) along the unit circuit, and the end point intersects with high Q circle (as shown in Figure 10). The target matching frequency is set through a ‘single’ variable inductor L and the impedance becomes Z_1 . Then, by applying the up-down symmetrical nature of Smith chart, a second series capacitor C_1 of the same value, $C_1=C_2=C$, pulls back from impedance Z_1 to the center point $Z_o = 50\ \Omega$ and completes the impedance matching at the desired frequency. The tuning antenna is operated at this band thereby. As the large C_1 and C_2 are applied, a low selectivity can be fulfilled theoretically as shown in the right part of Figure 10(b).

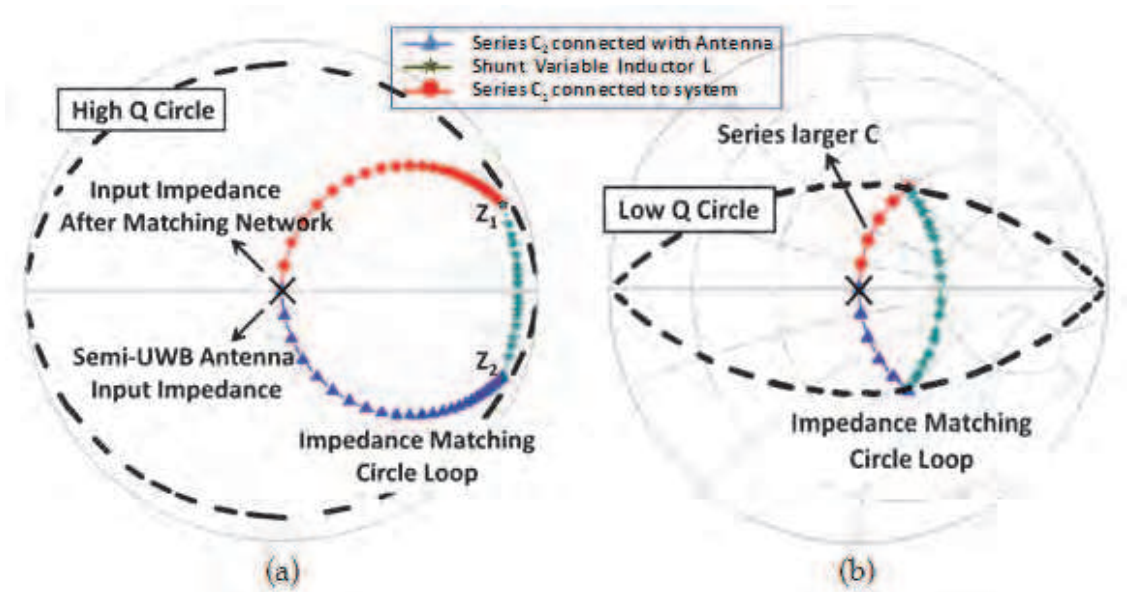


Fig. 10. Matching analysis on Smith chart with (a) High Q; (b) Low Q value.

An analytic formula for calculating the unknown inductance can be obtained as below, so the unknown inductance value L can be determined according to tunable matching frequency. T-type network impedance matching function can be observed from Figure 3 and is given as equation (3).

$$Z_0 = \left(\left(Z_{Ant} - \frac{j}{\omega C_2} \right)^{-1} - \frac{j}{\omega L_{total}} \right)^{-1} - \frac{j}{\omega C_1} \tag{3}$$

Applying the conditions of $Z_{ANT} \cong Z_o$, $C_1 = C_2 = C$ (constant), and the target frequency ω_{target} , and simplifying the equation, we get the equation (4) to obtain the inductor L_{total} .

$$L_{total} \approx \frac{1}{2} \left(CZ_0^2 + \frac{1}{(\omega_{target}^2 C)} \right) \tag{4}$$

where L_{total} is controlled by a varactor series with a fixed L to achieve well-matched at the frequency ω_{target} , and continuous tuning can be fulfilled by using a varactor, instead of discrete switching. We must apply the actual component values before it can comply with the predicted target frequency and find the precise frequency tuning ranges. Through basic thru-reflect-line (TRL) calibration technique, the values of the capacitance, the inductance and the parasitic impedance can be obtained precisely.

After we calculated the theoretical matching inductance, L_{total} , and the corresponding cascaded capacitance, C_{varactor} , the bias voltage value for the required capacitance can be determined from the varactor C-V curve we measured. Therefore, the variable inductor can be modeled with a proper varactor model which can be referenced in [Stauffer 2003]. The varying range of inductance is dominated by the varactor. This factor has thus determined the tunable ranges. In this chapter, a preliminary validation around 3 GHz is verified. The components are not optimized intentionally yet. Due to SMD component tolerance errors, the actual implemented operation frequency might be deviated. From the deviation status, the inductance differences are calibrated, and then the frequency deviation is compensated by correcting the bias voltage slightly to achieve the precise target frequency.

4. Implementation and experiment setup

To implement the proposed wide tuning antenna, three major parts are fabricated including an S-UWB antenna, a tunable matching network, and a controlling circuit. S-UWB antenna is fabricated without optimized fully-qualified performance. A circular-shaped antenna on FR4 ($\epsilon_r = 4.3$ and loss tangent $\delta=0.015$) substrate of 1.6 mm thickness is chosen and fabricated for demonstration as a simple design with an available wideband. Of course, other wideband antennas in different shapes are possible options. The relevant dimensions of S-UWB antenna are $[r/d/g/w_t] = 21.3/1/10/2.7$ mm and $[L_1/L_2/W] = 62/19/64$ mm. Those long transmission lines are extended for measurement and can be removed. The 'π'-shaped matching network is very small and attached at the interface of the antenna and RF front end. The frequency-tuning matching network is separated for the test purpose and it is feasible to fabricate nearly the antenna. The whole band-switchable tri-band antenna (analog antenna) and the transmission test is shown in Figure 11. Tri-band operation will be validated using Agilent NWA 8753E. Furthermore, we setup a UWB ridged horn to test path loss S_{21} using the proposed antenna. The orientation setup is based on the original the directivity of the S-UWB antenna.

The whole integrated reconfigurable antenna is shown in Figure 11, including the fabricated tunable matching network on Roger substrate (R04003C, $\epsilon_r = 3.55$, loss $\tan\delta=0.0021$) of 32 mil (0.81 mm) thickness. The component values are $C_1=C_2=0.6$ pF, $L_2=4.7$ nH, and $L_{\text{choke}}=7.8$ nH (for bias voltage input). The model number of GaAs hyperabrupt tuning varactor is MGV-125-23-E28, with a useable capacitance from 0.3 pF to 4 pF. The Q factor of the varactor is 3000, and its series resistance is about 1 Ω . The controlled circuitry is made by the micro-processor 89C51 to set a proper bias voltage on varactor through a DAC and an OP-Amplifier. The controlling module can be miniature using ASIC technologies in the future. The S_{11} of the reconfigurable antenna can be measured with the network analyzer Agilent N9020A. One double ridged UWB horn antenna (1 GHz ~ 18 GHz) is placed at a distance of 60 cm as the far field region to test the reception performance (S_{21}) of the tunable antenna.

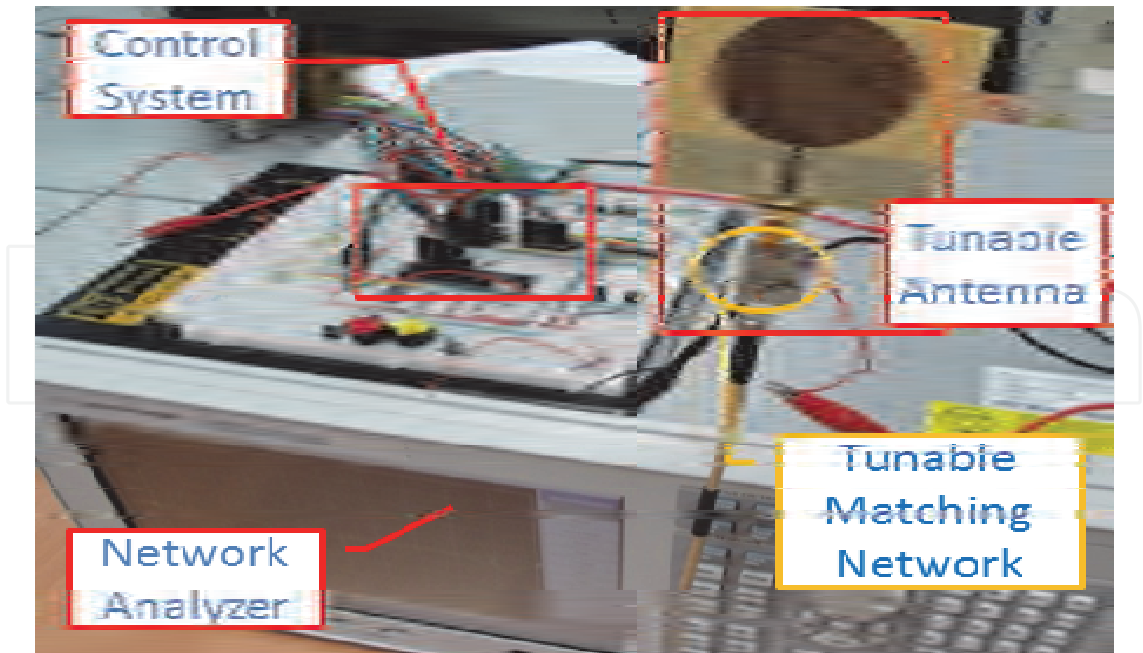


Fig. 11. The implemented reconfigurable S-UWB antenna attached with matching network.

5. Results and discussion

5.1 Simulation results of wide range for reconfigurable antennas

Table 3 shows the simulation results of antenna impedances; therefore, series inductor L and parallel inductor C is chosen correspondingly. Then, the W-USB antenna becomes a narrowband one and selects at frequencies 1.8, 2.4, 3.5, 5.8, 9, and 11.5 GHz as shown in Figure 12. This implies the proposed techniques can provide a very broad tunable range, which is very significant. The ratio is $11.5/1.8$ ($\sim 640\%$). In practice, the loss of the realistic matching network should be taken into account, so this is one of the reasons why S-UWB antennas are chosen so that the matching component can be realistic. For example, an antenna whose impedance contains a low resistive part and very high reactance is not good for matching implementation. Of course, while considering the practical parasitic effects, the tuning ratio will reduce, but it is still wide enough and will be shown in measurement.

Frequency(GHz)	1.8	2.4	3.5	5.8	9	11.5
$Z_{\text{antenna}}(\Omega)$	$15.678 + j0.93$	$39.05 + j13.52$	$17.12 + j21.11$	$15.03 + j13.63$	$33.87 - j30.55$	$26.43 - j7.95$
Parallel Cap, C_1 (pF)	1.969	0.474	0.119	0.255	0.953	0.145
Series Ind, L_2 (nH)	2.617	0.702	1.261	0.837	0.244	0.228

Table 3. Designing L-C values for specific frequencies.

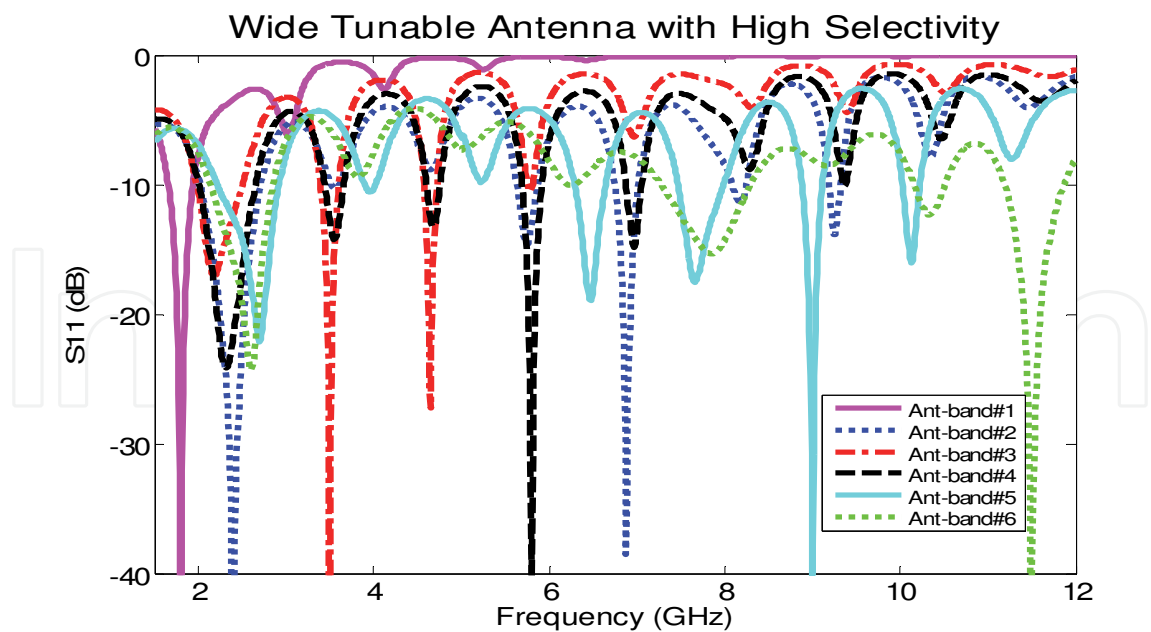


Fig. 12. The reconfigurable antenna can cover range from 1.8GHz – 11.5GHz.

5.2 Simulation results of high selectivity for reconfigurable antennas

Though at the desired frequency, the antenna can achieve high Q and good selectivity, however, from the Figure 13, there are some ripples falling into other bands which mean at these bands, the unwanted signals will leak into the receivers. Take 3.5 GHz-band as example, at 4.65GHz, S_{11} is also down to -25 dB, implying that the antenna can perform relatively well in transmitting and receiving at 4.65 GHz, which is not our design 3.5 GHz. This can be improved by changing the matching network from L-shaped to ‘ π ’-shaped or ‘T’-shaped. There will be one additional freedom to determine the Q factor, thereby other wanted parts can be eliminated. Figure 13 shows after applying $Cp_2/L/Cp_1$ of 7.958 pF / 0.448 nH / 5.85 pF values, the antenna again becomes very selective. Our proposed antennas do not have complicated design themselves but cooperate with the following matching network; multi-band reconfigurable antennas can be designed.

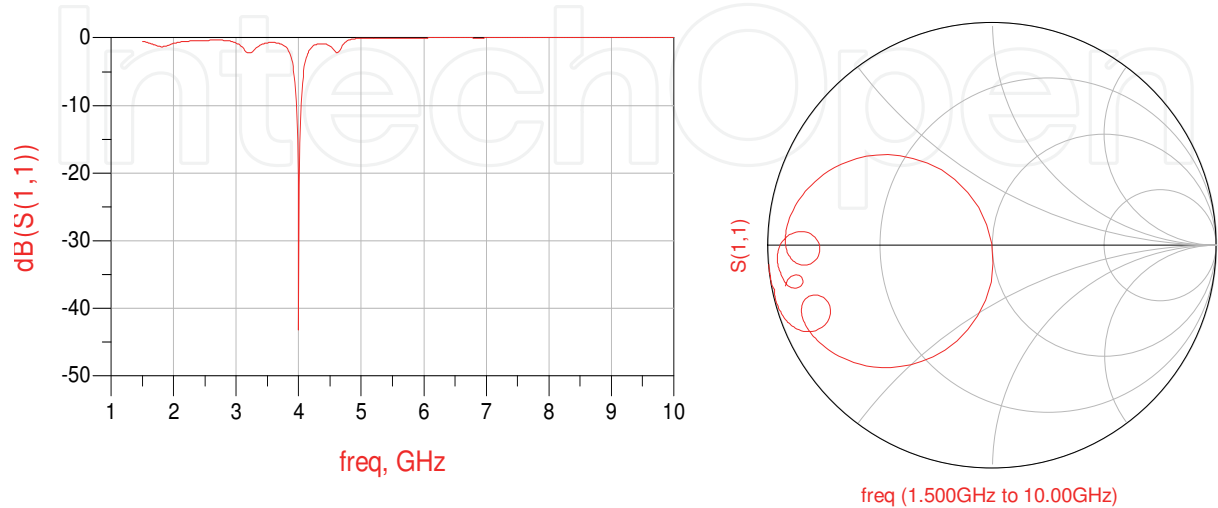


Fig. 13. Performance (S_{11} and the smith chart) using π -network at 4 GHz.

5.3 Measurement of fabricated tri-band antennas

Due to the manufacture variation of the lump elements, those calculated L/C values are tested separately to obtain its practical S-parameter model (S1P). After re-tuning according to these manufactured parameters and considering those transmission and switch influences carefully, the performance of the proposed tri-band antenna is shown in Figure 14. The dashed, solid, and dotted lines correspond to the ADS simulated results in different bands. Furthermore, this antenna keeps the flexibility of the tuning to the three bands without replacement of the S-UWB but the matching network components. Furthermore, if we add one set of the $C_1/L_2/C_3$ ($=5.06\text{pF}/0.397\text{nH}/4.11\text{pF}$) lump element values, we can expand this antenna into a quad-band antenna. This implies this fabricated antenna can be extended to a multiband antenna (more than four bands) easily with extremely low cost. However, close bands need extremely high-Q and precise components to isolate and it is not fulfilled in this work.

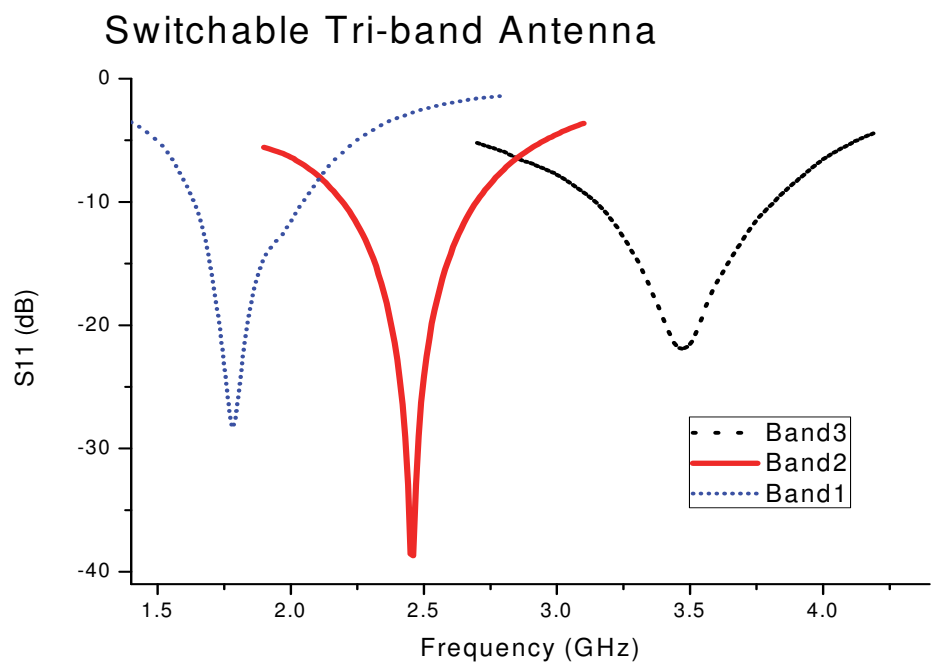


Fig. 14. S_{11} of the measured tri-band antenna.

5.4 Measurement of controllable bandwidth

As we mention in introduction, most of the multiband antenna is fixed and can be optimized the performance for their specific bands; however, it is relatively complicated to control the bandwidth. This may be useful for the adaptively data rate system for SDR or CR to minimize the noise floor power yet keep the SNR as large as possible. In our proposed architecture, we may use the frequency-tuning network in the traditional aspect; in other word, the frequency is fixed (for example, at $f_c = 2.45\text{GHz}$). Therefore, we may switch different L/C values in the π -shaped matching network to control its bandwidth. A fabricated circular S-UWB antenna is applied into the ADS simulations to obtain the L/C component values. The three cases of the bandwidths are demonstrated in Figure 15 using the values in Table 4. These results show the fractal bandwidths of 11%, 22%, and 33%.

$f_c = 2.45\text{GHz}$	$C_1(\text{pF})$	$L_2 \text{ (nH)}$	$C_3(\text{pF})$
Small Q	0.75	2.6	1
Big Q	2	2.9	2.4
Extreme Q	5	1.5	5.6

Table 4. The matching network to various antenna bandwidths.

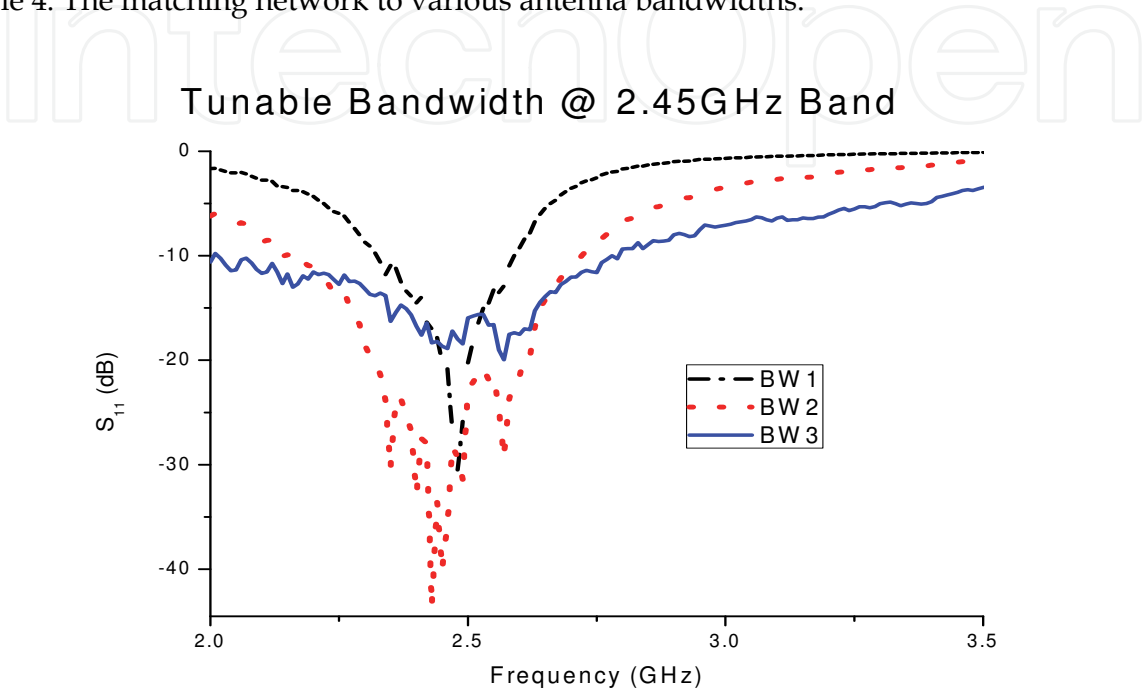


Fig. 15. A sample line graph using colors which contrast well both on screen and on a black-and-white hardcopy.

5.5 Measurement of continuously tuning for the reconfigurable antennas

An UWB horn antenna was used to compare S_{21} towards the S-UWB antenna itself with and without the frequency tunable matching network as the wideband and narrowband reception comparisons. First, the frequency tuning capability of the proposed antenna is verified and only a single controlling voltage is applied. The S_{11} measured results are shown in Figure 16. The components in the matching network are $C_1=C_2=0.6$ pF with two different series inductance (a) 4.7 nH and (b) 2 nH. The varactor is biased from 0 ~ 23 V. These tunable bands cover two different ranges, 1.8 GHz - 2.8 GHz (155%) and 2.19 GHz – 3.86 GHz (176%), respectively.

The matching network can change the original UWB frequency response to the narrowband operation at the desired frequency, so this S-UWB antenna is validated as the novel reconfigurable antenna. Moreover, our results show that only one desired band can be matched without other undesired matched bands and that ensures quality selectivity. The performance of the reconfigurable antenna can be listed in Table 5. This table shows the tunable range from 2.19 GHz to 3.86 GHz. The gain can be as low as -0.58 (up to -0.94 dB), which implies very low insertion loss.

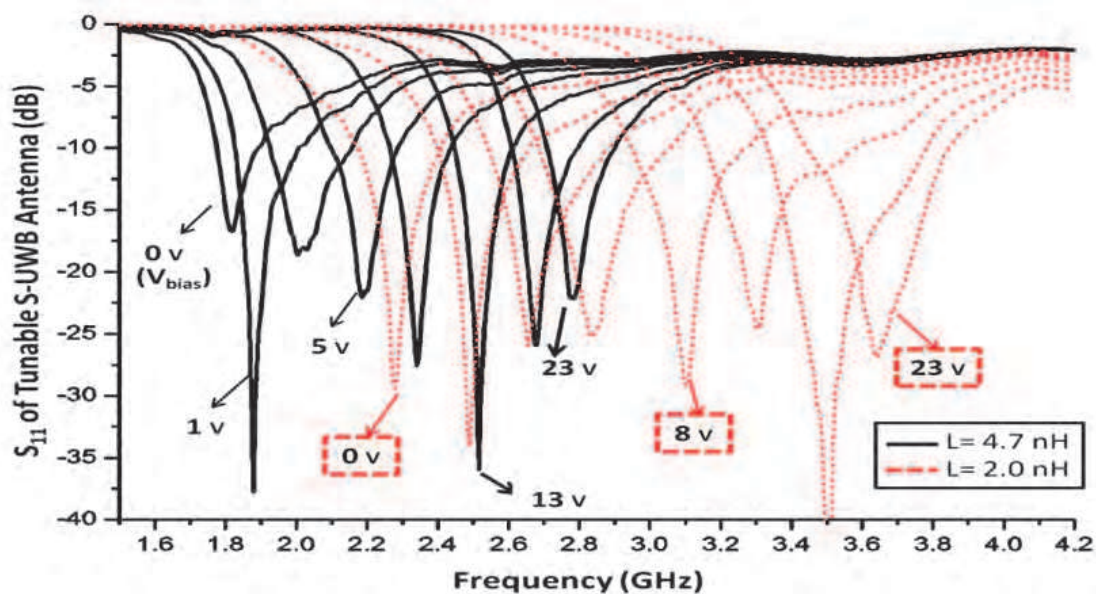


Fig. 16. Measured results of reconfigurable antenna S_{11} with biased voltage from 0 ~ 23 V; $C_1=C_2=0.6$ pF. $L= 4.7$ nH (solid line) or 2 nH (dashed line).

V_{bias} (volts)	0	1	2	5	10	15	23
Frequency (GHz)	2.19	2.31	2.78	2.97	3.44	3.73	3.86
Return Loss (dB)	-21.9	-30.3	-34.9	-38.2	-42.3	-20.7	-23
Gain (dB)	-0.94	-0.93	-0.89	-0.82	-0.7	-0.61	-0.58
BW (MHz)	288	240	239	300	432	324	222

Table 5. Performance of the reconfigurable antenna with $C_1/L/C_2 = 0.6$ pF/2 nH/0.6 pF.

6. Conclusion

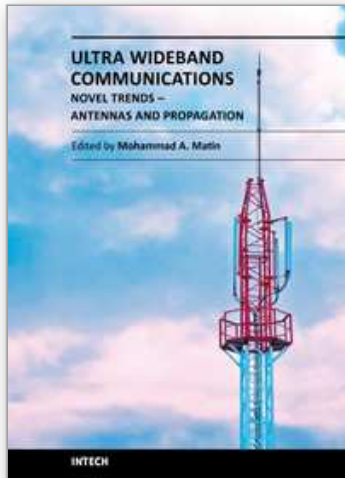
A novel band-switchable multi-band antenna is proposed by integrating a reconfigurable frequency-tuning matching network with an S-UWB antenna. Therefore, a tri-band (1.8/2.45/3.5 GHz) antenna is demonstrated. Moreover, the proposed multiband antenna not only has the features of switchable multiple bands and easy re-configuration, but also tunable bandwidth. 11% ~ 33% bandwidths are shown at 2.45 GHz. By using ideal components without parasitic effects, high selective antennas which cover ultra wide ranges from 1.8 GHz to 11.5GHz are achieved in simulation.

A procedure of handling practical lump components tolerate error is developed and calibrated to implement a tested prototype which is shown to match the predicted performance at operation frequencies. The measurement results show that the matching network features an average transducer power gain of -0.58~ -0.94 dB, which enables the antenna capable of tunable ratio of 163%, controlled by only one single bias voltage, and an average bandwidth of 300 MHz (from 2.5% to 9.6%). We have also investigated into the continuous controllable mechanism and overall improvement of Q value.

This chapter provides a wide and feasible method to apply the matching network as part of the reconfigurable antennas to expand their functions, to ease the design flow, and to reduce the implementation cost. Modifying the matching network can further tune to extra bands and different bandwidths and improves the flexibility of traditional multiband antennas. All these results recommend that this design concept is able to lower the process, time and analytical difficulty of the tunable antenna design significantly. The general analytical principle and design equations can be applied in any kind of wideband antennas. In the future, this design concept can be applied in designing and controlling multi-band tunable antennas as well.

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This book explores both the state-of-the-art and the latest achievements in UWB antennas and propagation. It has taken a theoretical and experimental approach to some extent, which is more useful to the reader. The book highlights the unique design issues which put the reader in good pace to be able to understand more advanced research.

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University Campus STeP Ri
Slavka Krautzeka 83/A
51000 Rijeka, Croatia
Phone: +385 (51) 770 447
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www.intechopen.com

InTech China

Unit 405, Office Block, Hotel Equatorial Shanghai
No.65, Yan An Road (West), Shanghai, 200040, China
中国上海市延安西路65号上海国际贵都大饭店办公楼405单元
Phone: +86-21-62489820
Fax: +86-21-62489821

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