Chapter 4

The Heat and Mass Transfer Analysis During Bunch Coating of a Stretching Cylinder by Casson Fluid

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Additional information is available at the end of the chapter

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Abstract

The aim of this study is to coat a stretching cylinder with the help of a liquid film spray. The Casson fluid has been chosen for the coating phenomena. The thickness of the liquid film has been used as variable, and the influence of heat and mass transmission under the impact of thermophoresis has been encountered in the flow field. The required pressure term for the spray pattern during variable thickness has mainly been focused. Using the suitable similarity transformations, the basic flow equations for the fluid motion have been converted into high-order nonlinear coupled differential equations. Series solutions of subsequent problem have been obtained using controlling procedure optimal approach. Important physical constraints of skin friction, Nusselt number, and Sherwood number have been calculated numerically and discussed. Other physical parameters involved in the problem, i.e., Reynolds number Re, Casson fluid parameter β_1, Prandtl number Pr, Lewis number *Le*, Brownian motion parameter N_b, and thermophoresis parameter N_t have been illustrated. The skin friction effect and its physical appearance are also included in this work. The convergence is checked by plotting h-curves. The emerging parameters are discussed by plotting graphs. The recent work is also compared with the published work.

Keywords: thin film spray, Casson nanofluid, stretched cylinder, heat and mass transfer, thermophoresis, HAM

1. Introduction

The relation among pressure and flow is an important phenomena which plays a vital role to understand the circulation of the blood in the human body and its sustainability. The approach of pressure [1] can bring a partial barrier in some areas of the smaller vessels due to the

thrilling change of the yield stress. The blood is equally a mixture of two fluids Casson and the other one is Newtonian fluid and studied by Srivastava and Saxena [2]. They focused on the effect of resistance created by the viscosity term and wall shear stresses. Later on, this fluid is studied by many researchers on the stretching surfaces for other industrial and engineering usages [3]. Mahdy [4] have examined the fluid motion over an extending cylinder considering Casson fluid. Hayat et al. [5] have examined the third-order fluid motion over an extending tube within the effect of MHD. Qasim et al. [6] have considered the slip flow of sighted ferrofluid over an extending cylinder. Sheikholeslami [7] has studied the suction idea considering nanofluid over an extended cylinder. Manjunatha et al. [8] have examined the radiation effect in a porous space using dusty fluid and stretching cylinder. Abdulhameed et al. [9] have examined the oscillatory flow phenomena using circular cylinder. Hakeem et al. [10] have studied the flow of Walter's B fluid over an extending sheet. Pandey et al. [11] have studied the Walter's B viscoelastic nanofluid film energetic from below. The interesting and fruitful applications of thin film are the wire and fiber coating, processing of food stuff, extrusion of polymer and metal, drawing of plastic sheets, continuous casting, fluidization of reactor, and chemical processing equipment. On the basis of these applications, researchers did a lot of work on it. Wang [12] was the main researcher who investigated liquid film on an unstable extending surface. Recently Tawade et al. [13] have investigated liquid film flow over an unstable extending surface with thermal radiation, in the existence of continuous magnetic field using numerical method. The liquid film flow considering non-Newtonian fluids proliferates in many life geographies which is used mostly in cylindrical shapes. Several researchers [14–17] investigated power-law fluid with unsteady extending surface using different cases. Megahe [18] and Abolbashari et al. [19] have scrutinized thin film flow of Casson fluid using slip boundary conditions. Recently Qasim et al. [20] have examined the liquid film flow of nanofluid considering Buongiorno's model.

The liquid film spray on a stretching sheet has also an important phenomena to coat the metals and increase their life. The idea of spray on the stretching surface is the study of Wang [21]. Recently Noor et al. [22] considered the thin film spray of nanofluid on a stretching cylinder. They compared their results with the experimental data and found the impact of the physical parameters during flow phenomena. They also discussed the application of their work in detail. Most of the mathematical problems in the field of engineering are composite in their nature, and the exact resolution is very tough or even not conceivable. The solution of these problems is tackled through numerical and analytical methods. Homotopy analysis method is one of the popular techniques for the solution of such complex problems. Liao [22–26] investigates this series solution technique for the solution of nonlinear problems. The other important feature of this method is that its solution contains all the embedded parameters involved in the problem and also the range of the embedded parameters. The high nonlinear problems have been solved by Abbasbandy [27] due to the fast convergence of this method. Alshomrani and Gul [28], Gul [29] have studied the solution of nonlinear differential equations through HAM arises in the field of engineering and industry.

2. Formulation

Consider the thin film flow of Casson nanofluid elegantly through a circular cylinder of radius "a." The cylinder is supposed to be stretched along with radial direction with velocity U_w, and

temperature at the surface of cylinder is taken T_w. The uniform ambient temperature is considered T_b such that $T_w - T_b > 0$ for assisting flow and $T_w - T_b < 0$ for opposing flow.

The governing equations of continuity, heat transfer, and mass transfer are

$$\frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial w}{\partial z} = 0, \tag{1}$$

$$u\frac{\partial w}{\partial r} + w\frac{\partial w}{\partial z} = \upsilon\left(1 + \frac{1}{\beta_1}\right)\left(\frac{\partial^2 w}{\partial r^2} + \frac{1}{r}\frac{\partial w}{\partial r}\right) + g\beta^*(T - T_b)(1 - C_b) + \frac{1}{\rho}(\rho^* - \rho)(C - C_b), \tag{2}$$

$$u\frac{\partial u}{\partial r} + w\frac{\partial u}{\partial z} = -\frac{1}{\rho}\frac{\partial P}{\partial r} + \upsilon\left(1 + \frac{1}{\beta_1}\right)\left(\frac{\partial^2 u}{\partial r^2} + \frac{1}{r}\frac{\partial u}{\partial r} - \frac{u}{r^2}\right), \tag{3}$$

$$u\frac{\partial T}{\partial r} + w\frac{\partial T}{\partial z} = \alpha\left(\frac{\partial^2 T}{\partial r^2} + \frac{1}{r}\frac{\partial T}{\partial r}\right) + \frac{\rho^* c_p^*}{\rho c_p}\left(D_B\frac{\partial T}{\partial r}\frac{\partial \phi}{\partial r} + \frac{D_T}{T_b}\left(\frac{\partial T}{\partial r}\right)^2\right), \tag{4}$$

$$u\frac{\partial C}{\partial r} + w\frac{\partial C}{\partial z} = D_B\left(\frac{\partial^2 C}{\partial r^2} + \frac{1}{r}\frac{\partial C}{\partial r}\right) + \frac{D_T}{T_b}\left(\frac{\partial^2 T}{\partial r^2} + \frac{1}{r}\frac{\partial T}{\partial r}\right), \tag{5}$$

where $u(r, z)$ and $w(r, z)$ are velocity components; ρ is density; υ is kinematic viscosity; β_1 is the constant characteristic to Casson fluid; β^* is the coefficient of thermal expansion; g is the gravitational acceleration along z-axis; T, T_b, C and C_b determine the temperature, ambient temperature, concentration, and ambient concentration, respectively; and α, D_T, D_B stands for the thermal diffusivity, thermophoresis diffusion coefficient, and Brownian diffusion coefficient.

The suitable boundary conditions are

$$u = U_w, w = W_w, T = T_w, C = C_w \quad at \quad r = a, \tag{6}$$

$$\mu\frac{\partial w}{\partial r} = \frac{\partial T}{\partial r} = \frac{\partial C}{\partial r} = 0, u = w\frac{d\delta}{dz} \quad at \quad r = b. \tag{7}$$

Here $U_w = -ca$ represents the suction and injection velocity, and $W_w = 2cz$ is the stretching velocity such that c represents the stretching parameter and δ is the thickness of fluid film.

The similarity transformations are used to alter the basic Eqs. (1)–(7) used in [22] as

$$u = -ca\frac{f(\eta)}{\sqrt{\eta}}, w = 2cz\ \frac{df}{d\eta}, T(z) = T_b - T_{ref}\left(\frac{cz^2}{\upsilon_{nf}}\right)\theta(\eta), C(z) = C_b - C_{ref}\left(\frac{cz^2}{\upsilon_{nf}}\right)\phi(\eta), \tag{8}$$

where

$$\eta = \left(\frac{r}{a}\right)^2.$$

In the case of the outer radius b of the flow, $\eta = \left(\frac{b}{a}\right)^2$.

Using these transformations in Eqs. (1), (2), (4)–(7), we obtained a set of dimensionless equations which is

$$\left(1+\frac{1}{\beta_1}\right)\left(\eta\frac{\partial^3 f}{\partial\eta^3}+\frac{\partial^2 f}{\partial\eta^2}\right)+\mathrm{Re}\left(f\frac{\partial^2 f}{\partial\eta^2}-\left(\frac{\partial f}{\partial\eta}\right)^2+\lambda\left(\theta+Nr\phi\right)\right)=0, \tag{9}$$

$$\eta\frac{\partial^2\theta}{\partial\eta^2}+\frac{\partial\theta}{\partial\eta}+\mathrm{Pr.Re}\left(f\frac{\partial\theta}{\partial\eta}-2\frac{\partial f}{\partial\eta}\theta\right)+\eta\frac{\partial\theta}{\partial\eta}\left(N_t\frac{\partial\theta}{\partial\eta}+N_b\frac{\partial\phi}{\partial\eta}\right)=0, \tag{10}$$

$$\eta\frac{\partial^2\phi}{\partial\eta^2}+\frac{\partial\phi}{\partial\eta}+Le.\mathrm{Re}\left(f\frac{\partial\phi}{\partial\eta}-2\frac{\partial f}{\partial\eta}\phi\right)+\frac{N_t}{N_b}\left(\eta\frac{\partial^2\theta}{\partial\eta^2}+\frac{\partial\theta}{\partial\eta}\right)=0, \tag{11}$$

where

$$\begin{aligned}&\mathrm{Re}=\frac{ca^2}{2\upsilon_{nf}},\ \lambda=\frac{g\beta^*a(T_w-T_\infty)(1-C_\infty)}{W_w^2},\ Nr=\frac{(\rho-\rho^*)(C_w-C_\infty)}{\rho\beta^*(T_w-T_\infty)(1-C_\infty)},\\&\mathrm{Pr}=\frac{\mu c_p}{k},\ N_t=\frac{\rho^*c_p^*D_T\Delta T}{\rho c_p\alpha T_b},\ Le=\frac{\upsilon}{D_B},\ N_b=\frac{\rho^*c_p^*D_B\Delta C}{\rho c_p\alpha}.\end{aligned} \tag{12}$$

In Eq. (12) Re stands for the Reynolds number, λ is the buoyancy parameter or in other word it is the natural convection parameter, Nr stands for the buoyancy ratio, Pr represents the Prandtl number, N_t is used to represent thermophoresis parameter, Le is Lewis number, and N_b is Brownian motion parameter.

Physical conditions for momentum, thermal, and concentration fields are transformed as

$$f(1)=\frac{\partial f(1)}{\partial\eta}=\theta(1)=\phi(1)=1, \tag{13}$$

$$\frac{\partial^2 f(\beta)}{\partial\eta^2}=f(\beta)=\frac{\partial\theta(\beta)}{\partial\eta}=\frac{\partial\phi(\beta)}{\partial\eta}=0, \tag{14}$$

where β is the thickness of liquid film sprayed on the outer surface of the cylinder.

Integrating Eq. (3) for pressure term

$$\frac{p-p_b}{\mu c}=\frac{\mathrm{Re}}{\eta}f^2-2\left(1+\frac{1}{\beta_1}\right)\frac{\partial f}{\partial\eta}. \tag{15}$$

At the outer surface, the shear stress of the liquid film is zero, i.e.,

$$\frac{\partial^2 f(\beta)}{\partial\eta^2}=0. \tag{16}$$

The shear stress on the cylinder is

$$\tau=\frac{\rho\upsilon 4cz}{a}f''(1)=\frac{4c\mu z}{a}f''(1) \tag{17}$$

The deposition velocity V is written as

$$-V = -ca\frac{f'(\beta)}{\sqrt{\beta}}. \tag{18}$$

Mass flux m_1 is in association with the deposition per axial length which is

$$m_1 = V2\pi b \tag{19}$$

The normalized mass flux m_2 is

$$m_2 = \frac{m_1}{2\pi a^2 c} = \frac{m_1}{4\pi \upsilon_{nf} \mathrm{Re}} = f(\beta) \tag{20}$$

The flow, temperature, and concentration rates are

$$S_f = \frac{2\upsilon_{nf}}{W_w}\left(\frac{\partial w}{\partial r}\right)_{r=a}, Nu = -\frac{ak}{(T_w - T_b)}\left(\frac{\partial T}{\partial r}\right)_{r=a}, Sh = -\frac{a}{2(C_w - C_b)}\left(\frac{\partial C}{\partial r}\right)_{r=a}. \tag{21}$$

The nondimensional forms for the abovementioned physical properties are

$$\frac{z\mathrm{Re}}{a}S_f = \frac{\partial^2 f(1)}{\partial \eta^2}, Nu = -2k\frac{\partial \theta(1)}{\partial \eta}, Sh = -\frac{\partial \phi(1)}{\partial \eta}. \tag{22}$$

3. Solution by homotopy analysis method

Initially guessed values for f, θ, and ϕ at $\eta = 1$ are

$$\begin{aligned} f_0(\eta) &= \frac{\beta}{2(\beta-1)^3}\left[\eta^3 - 3\beta\eta^2 - (3-6\beta)\eta + (2-3\beta)\right] + \eta, \\ \theta_0(\eta) &= \frac{-\eta^2}{2} + \beta(\eta - 1) + \frac{3}{2}, \phi_0(\eta) = \frac{-\eta^2}{2} + \beta(\eta - 1) + \frac{3}{2}. \end{aligned} \tag{23}$$

The linear operators for the given functions L_f, L_θ and L_ϕ are selected as

$$L_f = \frac{\partial^4 f}{\partial \eta^4}, \quad L_\theta = \frac{\partial^2 \theta}{\partial \eta^2} \quad \text{and} \quad L_\phi = \frac{\partial^2 \phi}{\partial \eta^2}, \tag{24}$$

which satisfies the following general solution:

$$L_f\left(A_1 + A_2\eta + A_3\eta^2 + A_4\eta^3\right) = 0, \quad L_\theta(A_5 + A_6\eta) = 0 \quad \text{and} \quad L_\phi(A_7 + A_8\eta) = 0, \tag{25}$$

where $A_i (i = 1 - 8)$ are constants of general solution.

The corresponding nonlinear operators N_f, N_θ, and N_ϕ are defined as

$$N_f[f(\xi;p),\theta(\xi;p)] = \left(1+\frac{1}{\beta_1}\right)\left(\eta\frac{\partial^3 f(\eta;p)}{\partial\eta^3}+\frac{\partial^2 f(\eta;p)}{\partial\eta^2}\right) + \mathrm{Re}\left(f(\eta;p)\frac{\partial^2 f(\eta;p)}{\partial\eta^2}-\left(\frac{\partial f(\eta;p)}{\partial\eta}\right)^2\right)+\left(\lambda\theta(\eta;p)+Nr\phi(\eta;p)\right)=0, \tag{26}$$

$$N_\theta[f(\xi;p),\theta(\xi;p)] = \eta\frac{\partial^2\theta(\eta;p)}{\partial\eta^2}+\frac{\partial\theta(\eta;p)}{\partial\eta}+\mathrm{Pr.Re}\left(f(\eta;p)\frac{\partial\theta(\eta;p)}{\partial\eta}-2\frac{\partial f(\eta;p)}{\partial\eta}\theta(\eta;p)\right) + \eta\frac{\partial\theta(\eta;p)}{\partial\eta}\left(N_t\frac{\partial\theta(\eta;p)}{\partial\eta}+N_b\frac{\partial\phi(\eta;p)}{\partial\eta}\right)=0, \tag{27}$$

$$N_\phi[f(\eta;p),\phi(\eta;p)] = \eta\frac{\partial^2\phi(\eta;p)}{\partial\eta^2}+\frac{\partial\phi(\eta;p)}{\partial\eta}+Le.\mathrm{Re}\left(f(\eta;p)\frac{\partial\phi(\eta;p)}{\partial\eta}-2\frac{\partial f(\eta;p)}{\partial\eta}\phi(\eta;p)\right) + \frac{N_t}{N_b}\left(\eta\frac{\partial^2\theta(\eta;p)}{\partial\eta^2}+\frac{\partial\theta(\eta;p)}{\partial\eta}\right)=0, \tag{28}$$

where $p\in[0,1]$ is embedded parameter.

4. Zeroth-order deformation problem

The equations of zeroth-order deformation problem are obtained as

$$(1-p)L_f\left[f(\eta;p)-f_0(\eta)\right]=ph_fN_f[f(\eta;p)], \tag{29}$$

$$(1-p)L_\theta[\theta(\eta;p)-\theta_0(\eta)]=ph_\theta N_\theta[f(\eta;p),\theta(\eta;p)], \tag{30}$$

$$(1-p)L_\phi\left[\phi(\eta;p)-\phi_0(\eta)\right]=ph_\phi N_\phi\left[f(\eta;p),\phi(\eta;p)\right]. \tag{31}$$

Here h_f, h_θ and h_ϕ are auxiliary nonzero parameters. The corresponding boundary conditions are written as

$$f(\eta;p)_{\eta=1}=1,\left.\frac{\partial f(\eta;p)}{\partial\eta}\right|_{\eta=1}=1,\theta(\eta;p)\big|_{\eta=1}=1,\phi(\eta;p)\big|_{\eta=1}=1, \tag{32}$$

$$\left.\frac{\partial^2 f(\eta;p)}{\partial\eta}\right|_{\eta=\beta}=0,\left.\frac{\partial\theta(\eta;p)}{\partial\eta}\right|_{\eta=\beta}=0,\left.\frac{\partial\phi(\eta;p)}{\partial\eta}\right|_{\eta=\beta}=0. \tag{33}$$

Since

$$p=0\Rightarrow f(\eta;0)=f_0(\eta)=\eta,\theta(\eta;0)=\theta_0(\eta)=1,\phi(\eta;0)=\phi_0(\eta)=1, \tag{34}$$

$$p = 1 \Rightarrow f(\eta;1) = f(\eta), \theta(\eta;1) = \theta(\eta), \phi(\eta;1) = \phi(\eta). \tag{35}$$

Using the Taylor's expansions of $f(\eta;p)$, $\theta(\eta;p)$ and $\phi(\eta;p)$ about $p = 0$ in Eqs. (28)–(31), we obtained

$$f(\eta;p) = f_0(\eta) + \sum_{w=1}^{\infty} f_w(\eta) p^w, \tag{36}$$

$$\theta(\eta;p) = \theta_0(\eta) + \sum_{w=1}^{\infty} \theta_w(\eta) p^w, \tag{37}$$

$$\phi(\eta;p) = \phi_0(\eta) + \sum_{w=1}^{\infty} \phi_w(\eta) p^w, \tag{38}$$

where

$$f_w(\eta) = \frac{1}{w!} \frac{\partial^w f\ (\eta;p)}{\partial \eta^w}\bigg|_{p=0}, \theta_w(\eta) = \frac{1}{w!} \frac{\partial^w \theta\ (\eta;p)}{\partial \eta^w}\bigg|_{p=0}, \phi_w(\eta) = \frac{1}{w!} \frac{\partial^w \phi\ (\eta;p)}{\partial \eta^w}\bigg|_{p=0}. \tag{39}$$

The convergence of series depends on h_f, h_θ, and h_φ. So let us suppose that series converges at $p = 1$ for some values of h_f, h_θ, and h_φ, then Eqs. (35)–(37) become

$$f(\eta) = f_0(\eta) + \sum_{w=1}^{\infty} f_w(\eta), \tag{40}$$

$$\theta(\eta) = \theta_0(\eta) + \sum_{w=1}^{\infty} \theta_w(\eta), \tag{41}$$

$$\phi(\eta) = \phi_0(\eta) + \sum_{w=1}^{\infty} \phi_w(\eta). \tag{42}$$

5. w^{th} order deformation problem

By taking w times derivatives of Eqs. (28)–(32) and then dividing by $w!$ as well as substituting $p = 0$, we obtained the following equations:

$$L_f\left[f_w(\eta) - \chi_w f_{w-1}(\eta)\right] = \hbar_f\ \Re_w^f(\eta), \tag{43}$$

$$L_\theta[\theta_w(\eta) - \chi_w \theta_{w-1}(\eta)] = \hbar_\theta\ \Re_w^f(\eta), \tag{44}$$

$$L_\phi\left[\phi_w(\eta) - \chi_w \phi_{w-1}(\eta)\right] = \hbar_\phi\ \Re_w^f(\eta), \tag{45}$$

where

$$\chi_w = \begin{cases} 0, & \text{if} \quad p \leq 1 \\ 1, & \text{if} \quad p > 1 \end{cases}.$$

$$\Re_w^f(\eta) = \left(1 + \frac{1}{\beta_1}\right)\left(\eta f'''_{w-1} + f''_{w-1}\right) + \mathrm{Re}\sum_{j=0}^{w-1}\left(f_{w-1-j} f''_j - f'_{w-1-j} f'_j\right) + \left(Gr_t \theta_{w-1} + Gr_c \phi_{w-1}\right), \tag{46}$$

$$\Re_w^\theta(\eta) = \eta\theta''_{w-1} + \theta'_{w-1} + \mathrm{Pr.Re}\sum_{j=0}^{w-1}\left(f_{w-1-j}\theta'_j - 2f'_{w-1-j}\theta_j\right) + \eta\theta'_{w-1}\sum_{j=0}^{w-1}\left(N_t\theta'_{w-1} + N_b\phi'_{w-1}\right), \tag{47}$$

$$\Re_w^\phi(\eta) = \eta\phi''_{w-1} + \phi'_{w-1} + Le.\mathrm{Re}\sum_{j=0}^{w-1}\left(f_{w-1-j}\phi'_j - 2f'_{w-1-j}\phi_j\right) + \frac{N_t}{N_b}\left(\eta\theta''_{w-1} + \theta'_{w-1}\right). \tag{48}$$

The related boundary conditions are

$$\begin{aligned} f_w(1) = f'_w(1) = \theta_w(1) = \phi_w(1) = 1, \\ f''_w(\beta) = \theta'_w(\beta) = \phi'_w(\beta) = 0. \end{aligned} \tag{49}$$

The general solution of Eqs. (42)–(44) is given by

$$\begin{aligned} f_w(\eta) &= e_1 + e_2\eta + e_3\eta^2 + f_w^*(\eta), \\ \theta_w(\eta) &= e_4 + e_5\eta + \theta_w^*(\eta), \\ \phi_w(\eta) &= e_6 + e_7\eta + \phi_w^*(\eta). \end{aligned} \tag{50}$$

Here $f_w^*(\xi)$, $g_w^*(\xi)$ and $\theta_w^*(\xi)$ represent the particular solutions, and the constant $A_i (i = 1 - 8)$ are determined from boundary conditions (49).

6. Discussion about graphical results

The purpose of this study is to enhance the heat and mass diffusion by choosing a thin-layer spray of the Casson nanofluid over a stretching cylinder. The physical configuration of the problem is shown in **Figure 1**. The solution of the problem has been obtained using the homotopy approach, and the main features for the convergence (h-curves) of homotopy analysis method (HAM) have been shown in **Figures 2** and **3**. These figures demonstrate the h-curves for velocity, temperature, and concentration fields, respectively. The impact of buoyancy parameter λ and buoyancy ratio Nr on velocity field is prescribed in **Figure 4**. Velocity grows with the rising values of λ because the natural convection parameter λ and momentum boundary layer are in direct relation. The similar effect for the rising values of N_r can be seen in **Figure 4**. The effect of thickness parameter β and Casson fluid parameter β_1 versus velocity field is shown in **Figure 5**. Increasing values of β generate friction force and decline the velocity field because the thicker flow creates hurdles in fluid motion, while the thin layer is comparatively fast flowing.

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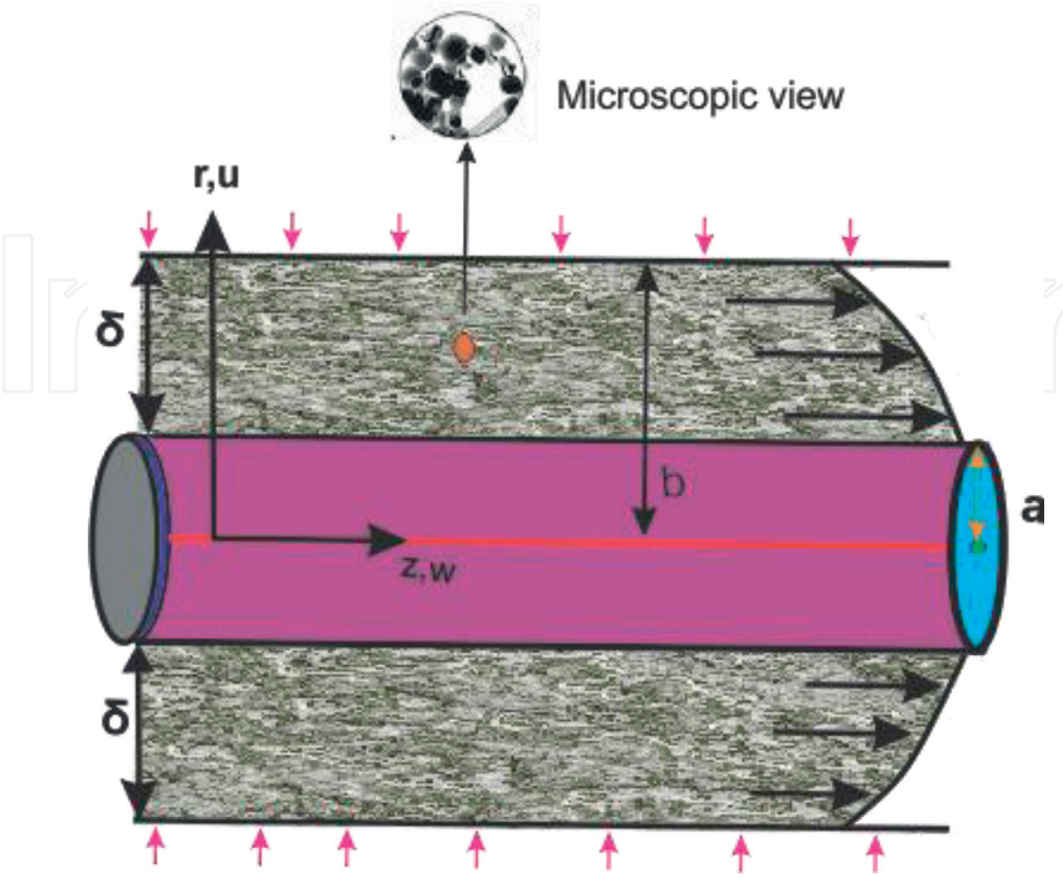

Figure 1. Physical geometry of the problem.

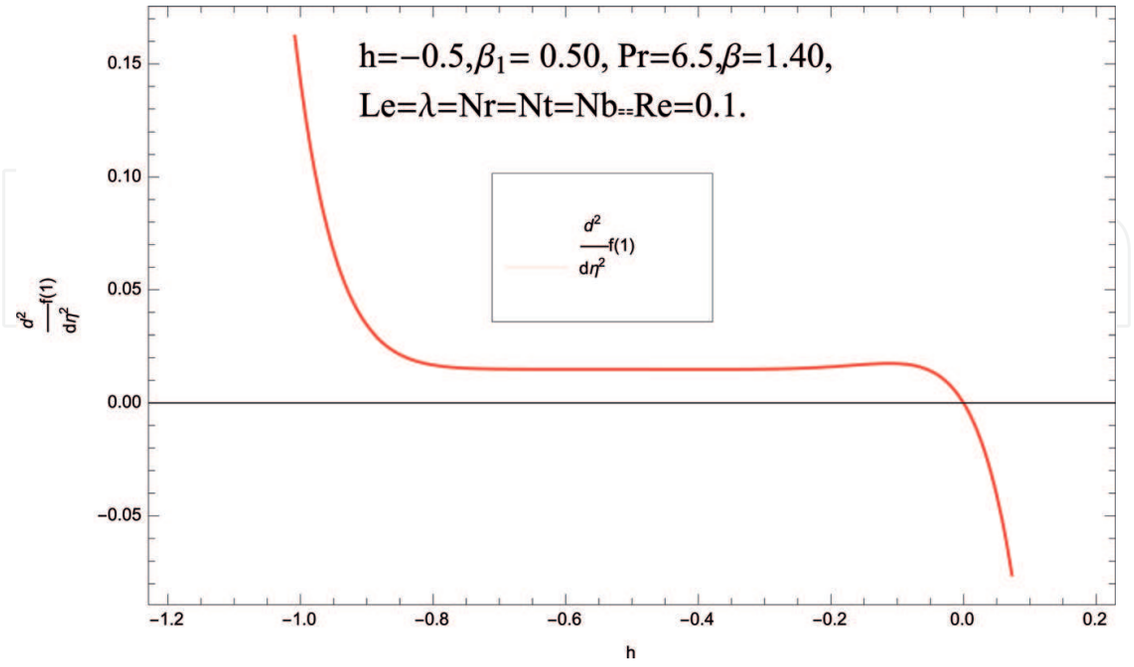

Figure 2. h-curve for velocity profile.

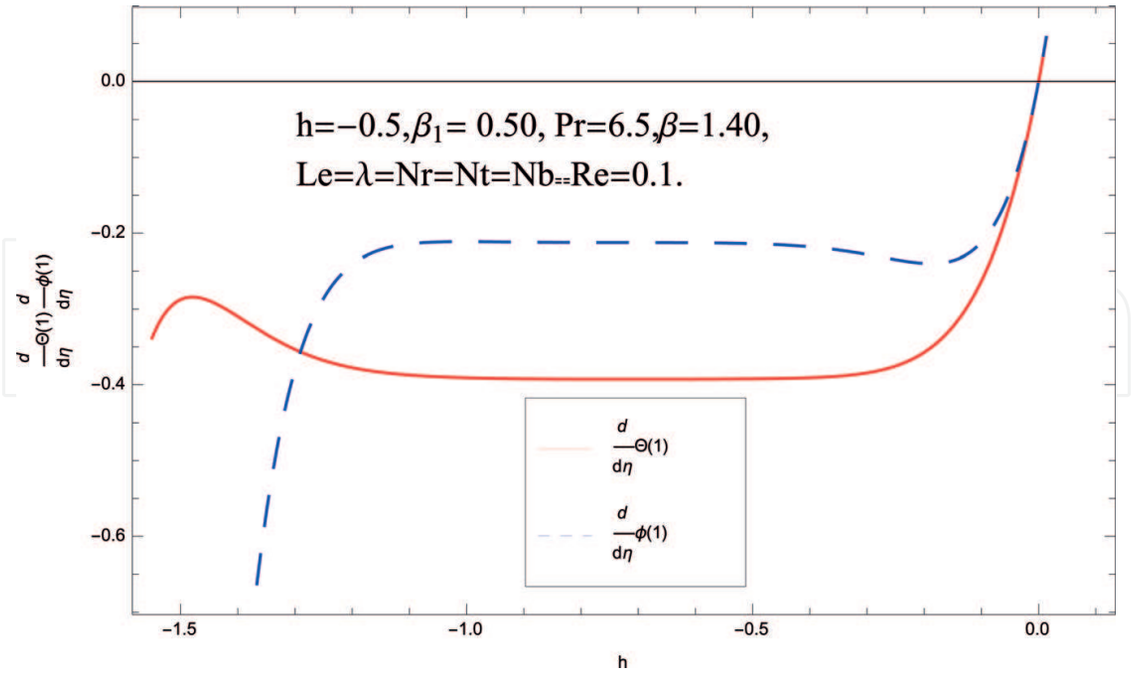

Figure 3. Combined h-curve for temperature and concentration fields.

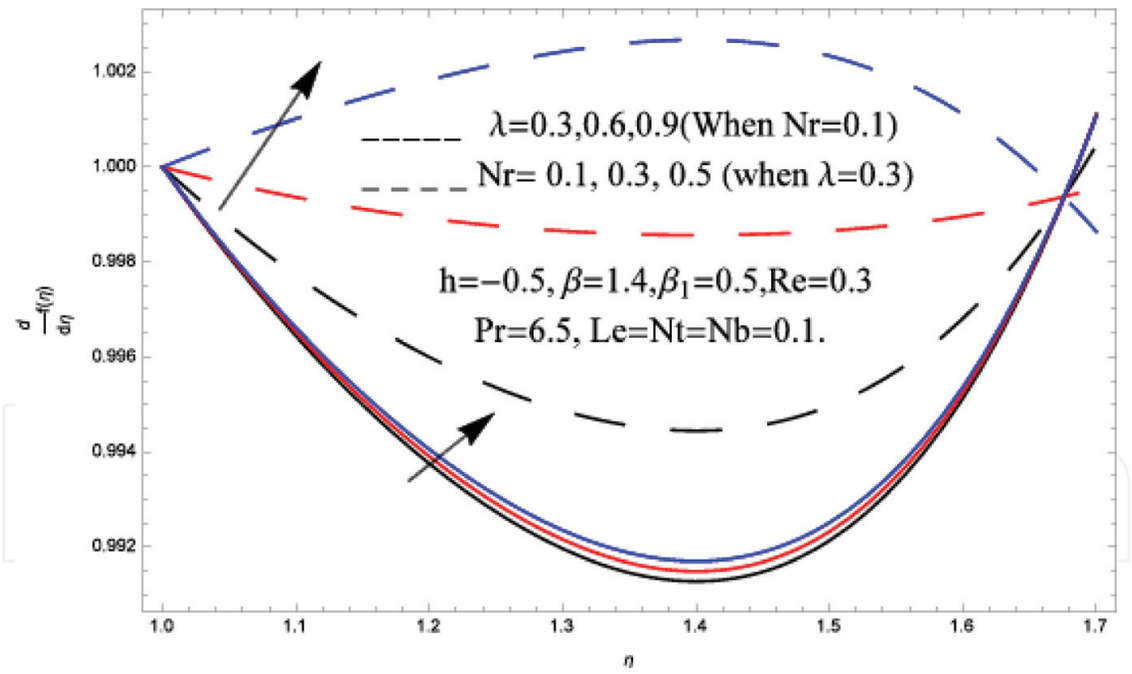

Figure 4. Variation of velocity with Nr and λ.

Therefore, larger amount of β declines the flow motion. The similar effect of the larger amount of the Casson fluid parameter β_1 is shown in **Figure 5**. The rising values of the parameter β_1 imply a decline in the yield stress of the Casson fluid. In **Figure 6**, the behavior of the thermophoretic parameter N_t and Reynolds number Re is observed over the field of temperature.

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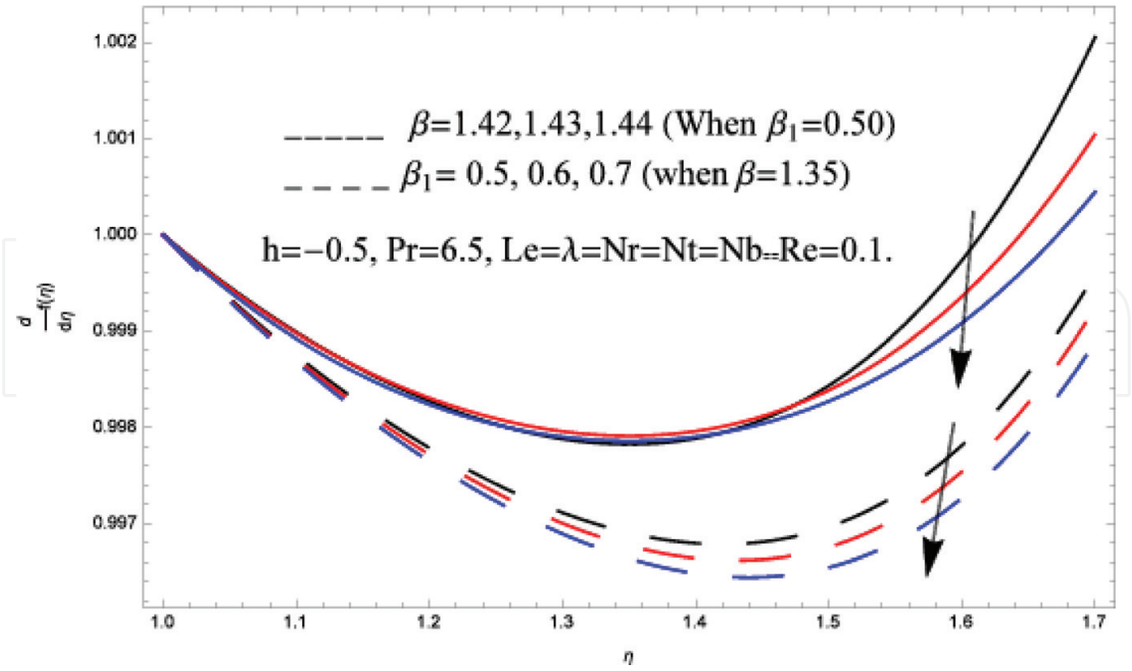

Figure 5. Variation of velocity with β and β_1.

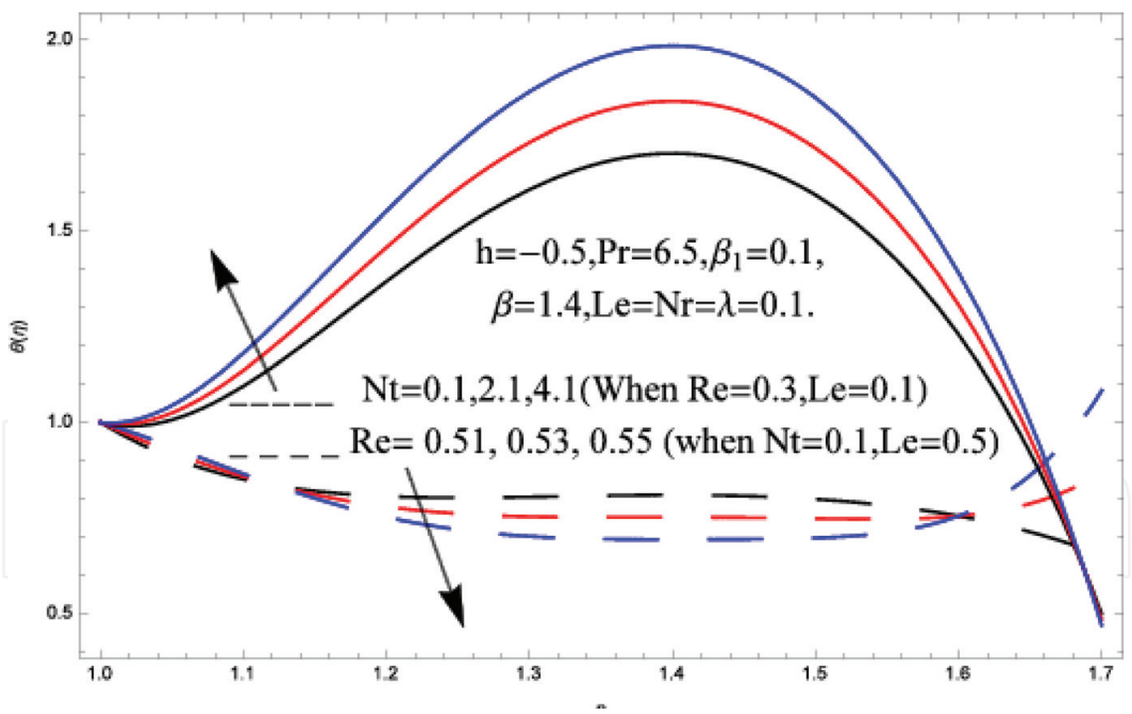

Figure 6. Variation of *Nt* and Re.

The larger amount of thermophoresis parameter N_t depreciates temperature profile because rising values of N_t enhance the concentration profile due to its direct relation and its product in the model equation increases the cooling effect to reduce the temperature field. The larger quantity of Re reduces temperature field. Rising values of Reynolds number Re enhance the

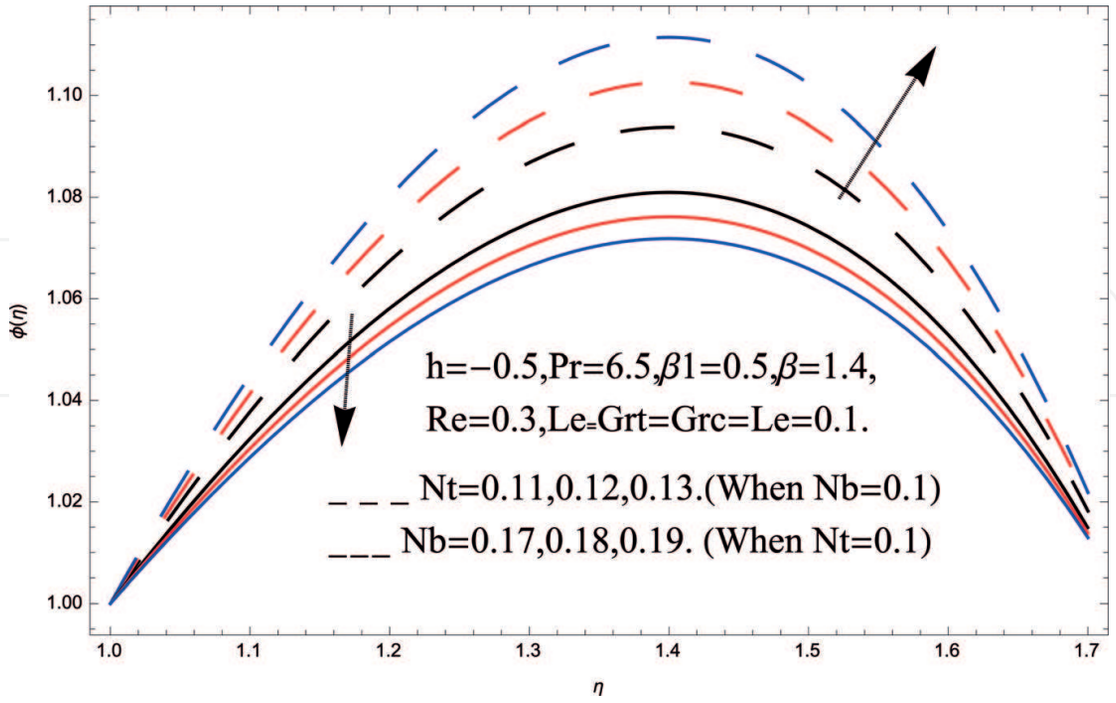

Figure 7. Variation of *Nt* and *Nb*.

inertial forces. The powerful inertial forces kept the fluid particles tightly closed, and more heat energy is required to break down the bonds among these atoms. In other words the inertial forces raise the boiling point of the fluid, and more heat energy is required to enhance the temperature. **Figure 7** shows the influences of thermophoretic parameter N_t and Brownian motion parameter N_b in concentration field. The larger amount of N_b displays a falling performance against concentration field. The parameter N_b is owing to the thinning of boundary layer because the random flow of liquid particles makes the decline in the concentration. The rising values of thermophoresis parameter N_t enhance the concentration field. The reason behind this is that N_t is in direct relation with concentration pitch, while the N_b is in inverse relation to the concentration field.

Figure 8 represents the behavior of the concentration field with respect to Reynolds number Re and Lewis number *Le*. The larger amount of Re improves the concentration field. The reason is that larger values of Re generate the enhancement in the inertial forces to rise concentration field. The concentration boundary layer is falling with the rising value of Lewis number *Le*.

Figure 9 shows the relationship between pressure distribution over the stretching surface versus Reynolds number Re and Casson fluid parameter β_1. The larger amount of β_1 increases the viscous forces, and more pressure are required at the surface. Thus the larger amount of β_1 decreases the pressure distribution. The larger amount of the Reynolds number Re decreases the pressure distribution. The strong inertial effects packed the fluid particle tightly, and as a result the pressure distribution decreases.

Table 1 shows the numerical values of the skin friction coefficient, local Nusselt number, and Sherwood number of various physical parameters. The skin friction coefficient rises with the

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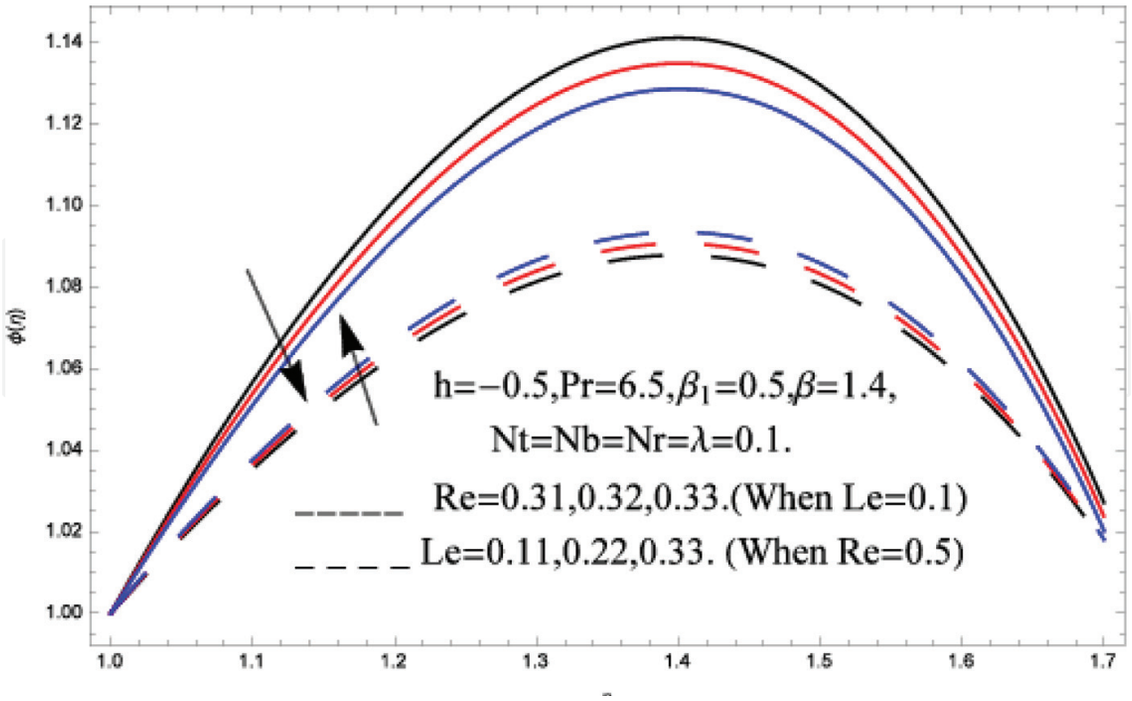

Figure 8. Variation of Re and *Le*.

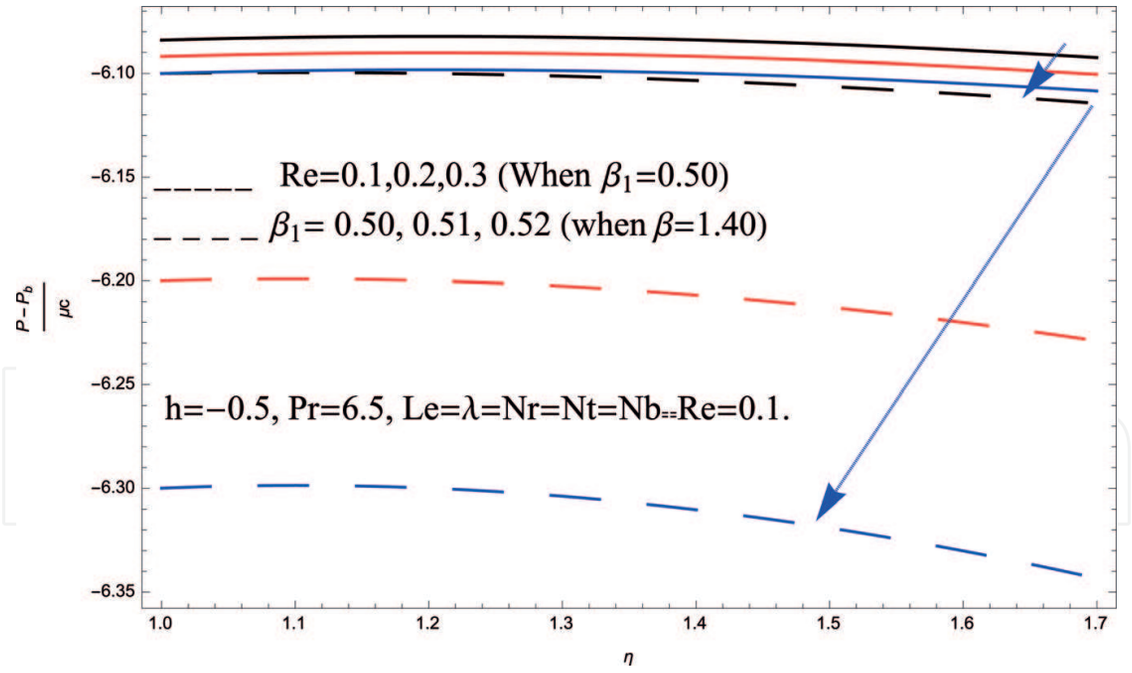

Figure 9. Variation of pressure term.

growth of thickness parameter β. The thick boundary layer increases friction force and improves the cooling effect. Therefore, the Nussselt and Sherwood numbers are increased. The Reynolds number Re decreases the fluid flow due to inertial forces. Due to this reason, the larger quantity of Re enhances the $f''(1), \Theta'(1)$ and $\phi'(1)$. Similar effect for rising values of the

β	Re	β_1	$f''(1)$	$\theta'(1)$	$\phi'(1)$
1.5	0.8	1.2	0.0149342	0.785646	0.212503
1.6			0.0150964	0.916634	0.260143
1.7			0.01673959	1.03338	0.309284
	0.8		0.0149342	0.785646	0.212503
	0.9		0.0151422	0.881567	0.240775
	1.0		0.0149653	0.976928	0.269410
		1.2	0.0149342	0.785646	0.212503
		1.3	0.0154906	0.785691	0.212518
		1.4	0.0160015	0.785733	0.212531

Table 1. Numerical values for skin friction coefficient, local Nusselt number, and Sherwood number for various physical parameters when $h = -0.5, Pr = 0.5, \beta_1 = 1.2, \beta = 1.5, Nt = 0.5, Nb = 1, Nr = 0.6, \mathrm{Re} = 0.8, Le = 0.5$.

Re	[30]	[31]	[4]	Present
0.5	0.88220	0.8827	0.88691	0.886942
1.0	1.17776	1.1781	1.17953	1.72926
2.0	1.59390	1.5941	1.59434	3.26714
5.0	2.41745	2.4175	2.4175	6.75053
10.0	3.34445	3.3445	3.34447	10.1078

Table 2. Values of $f''(1)$ for various Reynolds numbers when $h = -0.5, Pr = 0.5, \beta_1 = 1.2, \beta = 1.1, Nt = 0.5, Nb = 1, Nr = 0.6, Le = 0.5$.

Pr	[30]	[31]	[4]	Present
0.7	1.568	1.5683	1.56878	1.56846
2.0	3.035	3.0360	3.03596	3.68121
7.0	6.160	6.1592	6.15813	7.24452
10.0	10.77	7.4668	7.46477	10.2634

Table 3. Values of $-\theta'(1)$ for various Prandtl numbers when $h = -0.5, \beta_1 = 1.2, \beta = 1.1, Nt = 0.5, Nb = 1, Nr = 0.6, \mathrm{Re} = 0.8, Le = 0.5$.

Casson parameter β_1 has been shown in **Table 1**. The reason is that the viscous forces become dominant with the larger amount of β_1 to enhance the $f''(1)$, $\Theta'(1)$ and $\phi'(1)$. The comparison of present work and published work has been shown in **Tables 2** and **3**, and closed agreement for $f''(1)$, $\Theta'(1)$ and $\phi'(1)$ has been achieved.

7. Conclusion

The heat and mass transfer effect of a thin film over the extended surface of a cylinder has been explored in the recent research. The spray phenomenon has been studied in the form of

velocity, temperature, concentration, and pressure distribution profiles, respectively. The similarity transformation has been used to alter the governing equations into the set of nonlinear differential equations. The solution of the problems has been obtained through the homotopy analysis method (HAM). The impact of the embedded parameters has been examined and discussed. The outcomes of the recent study have been pointed out as:

- The inertial forces become stronger with the larger amount of Reynolds number Re, and as a result the velocity of the fluid flow reduces, while the upsurge values of Reenhance the $f''(1)$. Similarly, the Nusselt number and the Sherwood number are also increasing.
- The larger amount of the thickness parameter β of the thin film produces hurdles in the spray phenomenon, and as a result the velocity of the fluid decreases. On the other hand, the skin friction, Nusselt number, and the Sherwood number grow with the larger values of β. In fact, the cooling effect increases with the rising values of β to enhance the friction force.
- The greater amount of the Brownian motion parameter N_b declines the concentration field. The reason is that the rising values of N_b improve the thinning of the fluid layer and as a result the concentration profile reduces.
- The temperature field increases with the rising value of the thermophoresis parameter N_t, while the concentration field falls to reduce with the larger amount of N_t, because the thermophoresis parameter is in inverse relation to the concentration profile.
- The comparison of the present study with the published work authenticates the obtained result.

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